## **IASI-NG Level 1 processing**

# How to estimate the instrument spectral response function in real-time ?



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## **IASI – NG level 1 processing**



From IASI to IASI-NG: innovations and new challenges

Overview of the IASI-NG Level1 processing

The ISRF – Estimation Model

System performance budget



## **IASI-NG Level 1 main characteristics**

Main figures	IASI	IASI-NG
Radiometric Resolution (NeDT)		IASI/2
Spectral resolution	0.5 cm <sup>-1</sup>	IASI/2 (0.25 cm <sup>-1</sup> @L1C)
Absolute Radiometric Calibration	< 0,5K	IASI/2 (<0,25K@280K)
Spectral bands	3 bands	4 bands
Number of sounder pixels per acquisition	4 pixels	16 pixels
Ground Pixel diameter	12 km	12 km
Ground sampling	25 km	25 km



From IASI to IASI-NG: innovations and new challenges

- IASI vs IASI-NG? •
  - With great performance comes great complexity  $\rightarrow$





- 4 optical components
- 1 moving corner cube
- nearly achromatic / all reflective design
- 1 laser trigs the acquisition

F. Henault, C. Buil and al. - spaceborn infrared interferometer of the IASI instrument. Proc SPIE 3437, Infrared Spaceborn Remote Sensing VI. 18/11/1998



**IASI-NG** interferometer

- 6 optical components ٠
- 4 moving prisms, simultaneously
- chromatic and refractive design ٠
- 1 laser trigs the acquisition, 4 additionnal lasers for opd estimation ٠

plates

internal

nrisme

Mirror



cnes .

. .



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- IASI-NG ISRF estimation principle
  - ISRF is estimated <u>for every set</u> of 16x4 acquisitions

estimating the ISRF = knowing the science opd

Airbus D&S shows that the opd for every wavelength in the science band can be approximated by a linear combination of the 5 metrologies opd :

$$opd(\sigma) = \left(A_{cal}(\sigma) - C_0(\sigma, Z_0)\right) \cdot Z_0 + \sum_{i=1}^4 C_i(\sigma, Z_0) \cdot Z_i + OFFSET(\sigma, Z_0)$$

- $\mathbf{Z}_{i=1..4}$  : metrologies opd
- Z<sub>0</sub> : reference metrology opd
- $C_{i=0..5}$  : opd coefficients



- IASI-NG ISRF estimation principle
  - ISRF-Estimation Model parameters Coefficients

$$opd(\sigma) = \left(\frac{A_{cal}(\sigma)}{-C_0(\sigma, Z_0)}\right) \cdot Z_0 + \sum_{i=1}^{4} \frac{C_i(\sigma, Z_0)}{-C_i(\sigma, Z_0)} \cdot Z_i + \frac{OFFSET(\sigma, Z_0)}{-C_i(\sigma,$$

 $\mathbf{Z}_{i=1..4}$  : metrologies opd

They are a combination of :

- Z<sub>0</sub> : reference metrology opd
- $C_{i=0..5}$  : opd coefficients

**Computed coefficients** 

- Using a numerical model of the interferometer
- Parameters of the model can be updated in-orbit using WFS

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- **IASI-NG ISRF estimation principle** •
  - ISRF-Estimation Model parameters Coefficients

$$opd(\sigma) = \left(\frac{A_{cal}(\sigma)}{-C_0(\sigma, Z_0)}\right) \cdot Z_0 + \sum_{i=1}^4 \frac{C_i(\sigma, Z_0)}{-C_i(\sigma, Z_0)} \cdot Z_i + \frac{OFFSET(\sigma, Z_0)}{-C_i(\sigma, Z_$$

 $\begin{array}{c} Z_{i=1..4} \\ Z_0 \end{array}$ : metrologies opd

They are a combination of :

- : reference metrology opd
- $C_{i=0..5}$ : opd coefficients

#### Measured coefficient

- On-ground spectral shift (first guess) •
- In-orbit determination using ٠ dedicated acquisitions sequences (atmospheric spectra correlation + FPI)



- IASI-NG ISRF estimation principle
  - ISRF-Estimation Model parameters Coefficients A<sub>cal</sub>

The  $A_{cal}$  coefficient is related to the spectral shift  $\Delta\sigma$  throught the simple relation :

$$A_{cal}(\sigma) = \frac{\Delta\sigma}{\sigma}$$

1-  $A_{cal}(\sigma)$  values are computed for few wavenumbers (anchor points) across the IASI-NG band using correlation between observed and modeled spectra.





- IASI-NG ISRF estimation principle
  - ISRF-Estimation Model parameters Coefficients A<sub>cal</sub>

FPI plates (ZnSe) Winlight optics

The  $A_{cal}$  coefficient is related to the spectral shift  $\Delta\sigma$  throught the simple relation :



How on board calibrations will allow high level of performance during IASI-NG Mission E. Baldit and al – Poster session – Joint EUMETSAT/AMS/NOAA conf. 2019 (Boston)

$$A_{cal}(\sigma) = \frac{\Delta\sigma}{\sigma}$$



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- IASI-NG ISRF estimation performances
  - Preliminary assessments of ISRF estimation model are very promising :

#### Knowing the science opd = estimating the ISRF

Without defects, the opd estimation is better than few tenth of nanometers ( $\sim 1/1000$  OPD sampling)



- IASI-NG ISRF estimation performances
  - Preliminary assessments of ISRF estimation model are very promising :

#### Knowing the science opd = estimating the ISRF

#### opd variations induced by kinematical defects are also well corrected



Sensitivity of the opd error - translation defect

Sensitivity of the opd error below :

- **3nm/µm of translation** for every component / every wavenumbers
- Movement of 1µm of the compensating plate corresponds to a worst case

6 optical components x 3 transations / rotations

- The current budget of system performances shows very encouraging results in terms of
  - ✓ Geometric performances
  - Spectral performances
  - Radiometric performances











## Thank you ...





# 5<sup>th</sup> IASI Conference, 20-24 April 2020, Evian (France)











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## **Back-up slides**



From IASI to IASI-NG: innovations and new challenges

### **Applications are the same:**



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 $H_20$ 

 To deal with the stronger requirements in terms of performances, a new instrumental concept has been proposed:

- The Mertz interferometer allows a field compensation (self-apodisation correction)
- Field compensation is achieved by introducing optics with correct optical index
- A single 'dual swing" mechanism translates two pairs of prisms proportionally and creates simultaneously the OPD change and the self-apodisation compensation
- The level 1 processing has been modified consequently, especially to estimate the Instrument Spectral Response Function (ISRF)



Reflected



- Why estimate the instrument spectral response function (ISRF) ?
  - $\rightarrow$  The impact of the instrument on measured spectra

## **ISRF = response of the instrument to a spectral dirac**



input dirac



FM1 IFM Model (courtesy Airbus)



ISRF

## **The ISRF – Estimation Model**

- Why estimate the instrument spectral response function (ISRF) ?
  - $\rightarrow$  The impact of the instrument on measured spectra

## **ISRF = response of the instrument to a spectral dirac**



input dirac



FM1 IFM Model (courtesy Airbus)



ISRF



## **The ISRF – Estimation Model**

number (cm<sup>-</sup>

2500

2000

wavenumber [cm<sup>-1</sup>]

- Why estimate the instrument spectral response function (ISRF) ?
  - $\rightarrow$  The impact of the instrument on measured spectra



#### **ISRF = response of the instrument to a spectral dirac**

input spectrum

1500

1000

0.0010

0.0008

0.0006

0.0004

0.0002

0.0000



- Why estimate the instrument spectral response function (ISRF) ?
  - $\rightarrow$  The impact of the instrument on measured spectra



#### **ISRF = response of the instrument to a spectral dirac**



- IASI-NG ISRF defects
  - → Instrument impact on ISRF can be separated into 2 main categories :
  - > Defects induce by the gap between the realized instrument and the ideal ones :
    - optics realization (MSE,...),
    - alignments,
    - cinematic perturbations during the stroke, ...
    - ...
  - > Defects induce even if the instrument were ideal :
    - variable spectral shift due to the opd chromaticity

(~20cm<sup>-1</sup>@645 and ~12cm<sup>-1</sup>@2760cm<sup>-1</sup>)



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- IASI-NG ISRF estimation performances
  - Preliminary assessments of ISRF estimation model are very promising :

spectral shift estimation is below the **1.10**<sup>-6</sup> requirements when considering around 40 tropical (night/sea) atmospheric spectra (correlated with ref. mean tropical atmos.)



- IASI-NG ISRF estimation principle
  - ISRF-Estimation Model parameters Coefficients

$$opd(\sigma) = \left(\frac{A_{cal}(\sigma)}{-C_0(\sigma, Z_0)}\right) \cdot Z_0 + \sum_{i=1}^4 \frac{C_i(\sigma, Z_0)}{-C_i(\sigma, Z_0)} \cdot Z_i + \frac{OFFSET(\sigma, Z_0)}{-C_i(\sigma, Z_$$

 $Z_{i=0..4}$  : metrologies opd  $Z_5 = 1$  $C_{i=0..5}$  : opd coefficients

Measured coefficient :



(atmospheric spectra correlation +

They are a combination of :



#### **Computed coefficients**

- Using a numerical model of the interferometer
- Parameters of the model can be updated in-orbit using WFS

• Synthesis of the current performances budget (compared to specifications at mission level) for the main requirements

Description	Specified value / calculated value	Status
ISRF shift knowledge	1E10-6 / 1E10-6	compliant
ISRF shape error index	0.25% / 0.27% (parasitic contribution)	Marginally NC
Interpixel ISRF stability	1E10-4 / 3.3E10-5	compliant
Radiometric noise	See previous figure	compliant
Absolute radiometric calibration	0.25 K (O) and 0.5 K (T) / 0.24K	compliant
PSF uniformity knowledge	+/- 10 % / 14%	compliant
PSF characterization	-	No budget available
Spatial resolution	11.5 +/- 0.5 km / 11.8km	compliant
Ground sampling	3mrad / 3.2mrad	NC in worst case (compliant in typical case)
Pointing knowledge	+/- 3 mrad / 0.9mrad	compliant
Pointing accuracy	+/- 3 mrad / 0.91mrad	compliant
Pointing stability	0.1 mrad / 0.062 mrad	compliant
Sounder geolocation	1km / 949 m	compliant
Geolocation in degraded case	5km / 1108 m	compliant