



# Community Radiative Transfer Model (CRTM) Applications to Support Sensor Cal/Val and EDR Generations

**Quanhua (Mark) Liu<sup>1</sup>, Benjamin Johnson<sup>2</sup>,  
Tong Zhu<sup>2</sup>, Ming Chen<sup>3</sup>, and Yong Chen<sup>3</sup>**

1. NOAA/NESDIS Center for Satellite Applications and Research, College Park, Maryland
2. Joint Center for Satellite Data Assimilation, College Park, Maryland
3. University of Maryland, College Park, Maryland

**November 29, 2017**

# The first and the last emails from Paul vanDelst

From Paul Van Delst  
Subject Bryan Baum - Cirrus Modeling  
To Me  
Cc Yong Han <Yong.Han@noaa.gov>

3/30/2005 3:30 PM

To protect your privacy, Thunderbird has blocked remote content in this message.

Hi Quanhua,

This is the page I mentioned before about the ice crystal work in the infrared at Wisc.

<http://www.ssec.wisc.edu/~baum/Cirrus/IceCloudModels.html>

Do you see anything in this that we can use in the CRTM? I'm going to have a closer look at it next week, but you're the scattering expert so I figured you might have some pointers as to what is important.

cheers,

paulv

--  
Paul van Delst  
CIMSS @ NOAA/NCEP/EMC

From Paul Van Delst  
Subject CRTM solar/visible flag change in CRTM\_AMOM\_Layer procedures.  
To Tong Zhu - NOAA Affiliate <tong.zhu@noaa.gov>  
Cc Me

4/12/2016 2:34 PM

Hello,  
The problem is with the CRTM\_AMOM\_Layer[XXX] routines in ADA\_Module.

The lines where we have

```
IF( RTV%Visible_Flag_true ) THEN
```

should perhaps be

```
IF( RTV%Solar_Flag_true ) THEN
```

```
?
```

Here are the actual lines in the current trunk:

```
CRTM_AMOM_layer():  
https://svnemc.ncep.noaa.gov/trac/crtm/browser/trunk/src/RTSolution/ADA/ADA\_Module.f90#L391
```

```
CRTM_AMOM_layer_TL():  
https://svnemc.ncep.noaa.gov/trac/crtm/browser/trunk/src/RTSolution/ADA/ADA\_Module.f90#L825
```

```
CRTM_AMOM_layer_AD():  
https://svnemc.ncep.noaa.gov/trac/crtm/browser/trunk/src/RTSolution/ADA/ADA\_Module.f90#L1255
```

Please confirm that these are the correct ones to change.

cheers,

paulv

# Paul's Final Work on CRTM Cloud Data Assimilation

The computer codes Paul left for us are still working daily for this community. He will live on in our memories forever!

$$C_k = \frac{F_k}{G_k}$$

$$F_k = F_{k-1} + W_k f_k$$

$$G_k = G_{k-1} + W_k$$

$$\delta F_k = \delta F_{k-1} + W_k \delta f_k + f_k \delta W_k$$

$$\delta^* W_k = \delta^* W_k + f_k \delta^* F_k$$

$$\delta^* F_k = \delta^* f_k + W_k \delta^* F_k$$

$$\delta^* F_{k-1} = \delta^* F_{k-1} + \delta^* F_k$$

$$\delta^* F_k = 0$$

$$\delta G_k = \delta G_{k-1} + \delta W_k$$

$$\delta^* W_k = \delta^* W_k + \delta^* G_k$$

$$\delta^* G_{k-1} = \delta^* G_{k-1} + \delta^* G_k$$

$$\delta^* G_k = 0$$

$$\delta C_k = \frac{G_k \delta F_k - F_k \delta G_k}{G_k^2}$$

$$= \frac{1}{G_k} \delta F_k - \frac{F_k}{G_k^2} \delta G_k$$

$$\delta^* G_k = \delta^* G_k - \frac{F_k}{G_k^2} \delta^* C_k$$

$$\delta^* F_k = \delta^* F_k + \frac{1}{G_k} \delta^* C_k$$

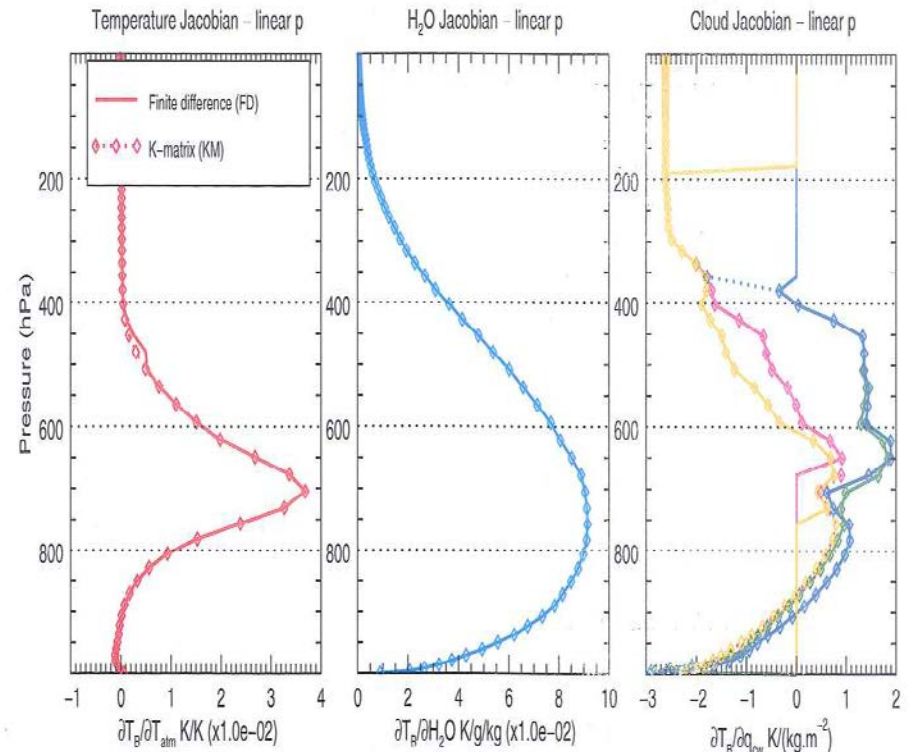
$$\delta^* C_k = 0$$

Every line he coded was just like his personality: neat, clean and clear; Every module he designed was just like his attitude toward life: making the optimum trade-off among different resources in order to pursue the best of the whole system.

## 2 CODE TESTING

### 2.3 Finite-difference and K-matrix Jacobian comparisons

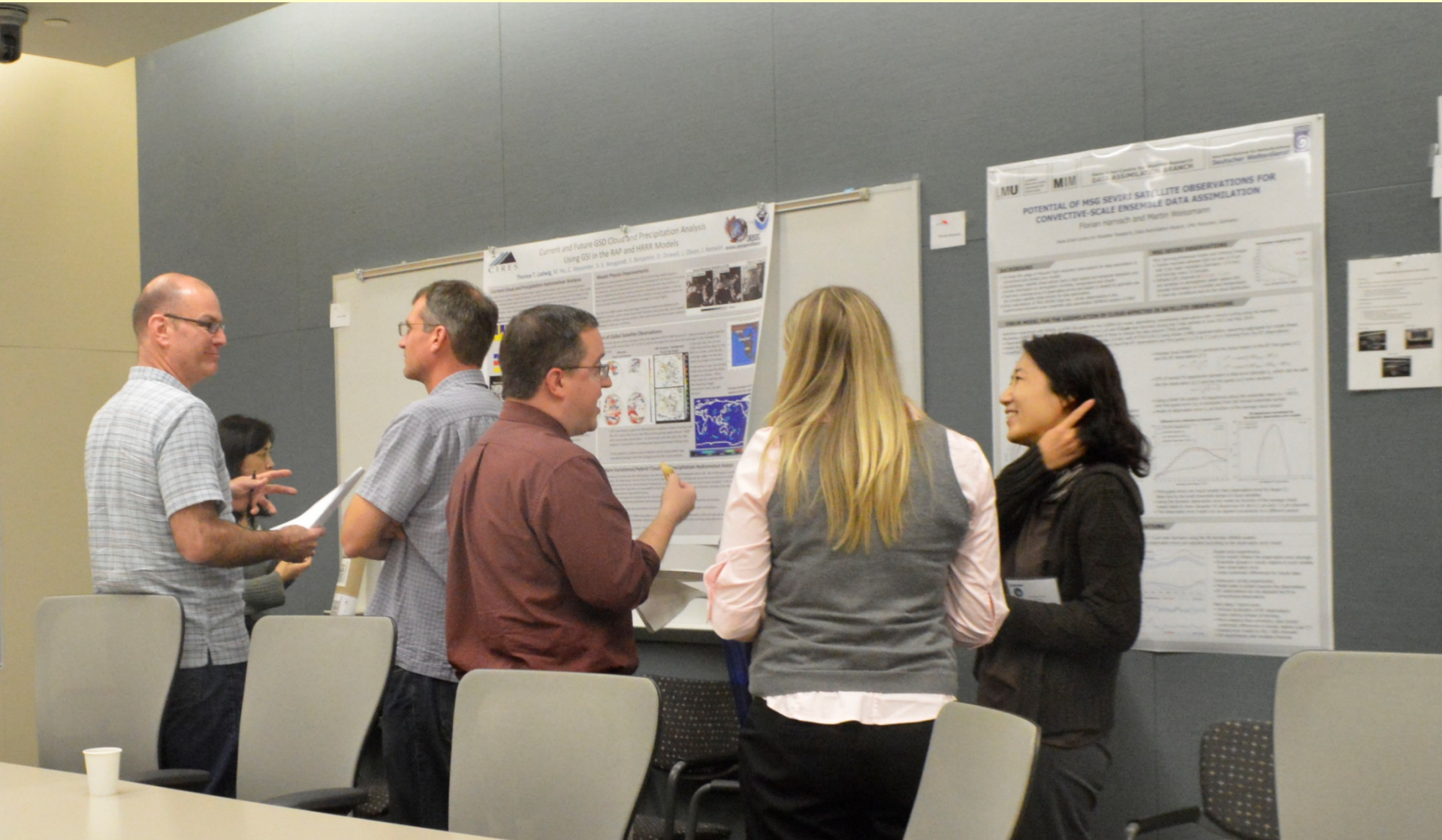
Figure 2.13: Comparison of NPP ATMS channel 2 finite-difference and K-matrix  $T_B$  Jacobians for ECMWF5K profile 1 using the cloud water amount weighted average method to compute fractional cloud cover. (Top) Temperature, water vapour, and cloud water content Jacobians. The colours for the latter represent water, ice, rain, and snow clouds. (Bottom) Channel brightness temperatures. Channel 2 is highlighted by the vertical green line.





# Paul vanDelst at JCSDA Annual Meeting

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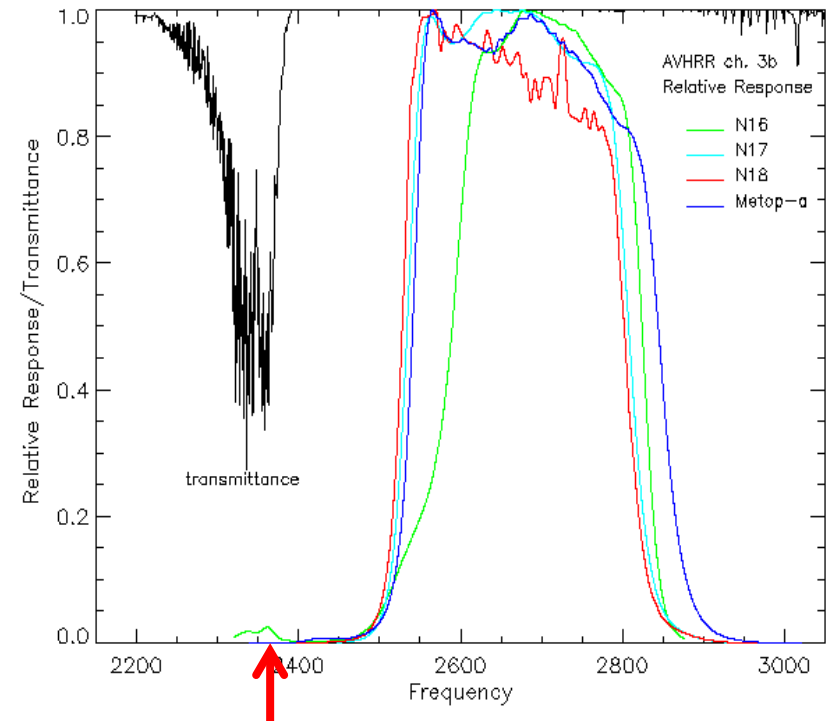
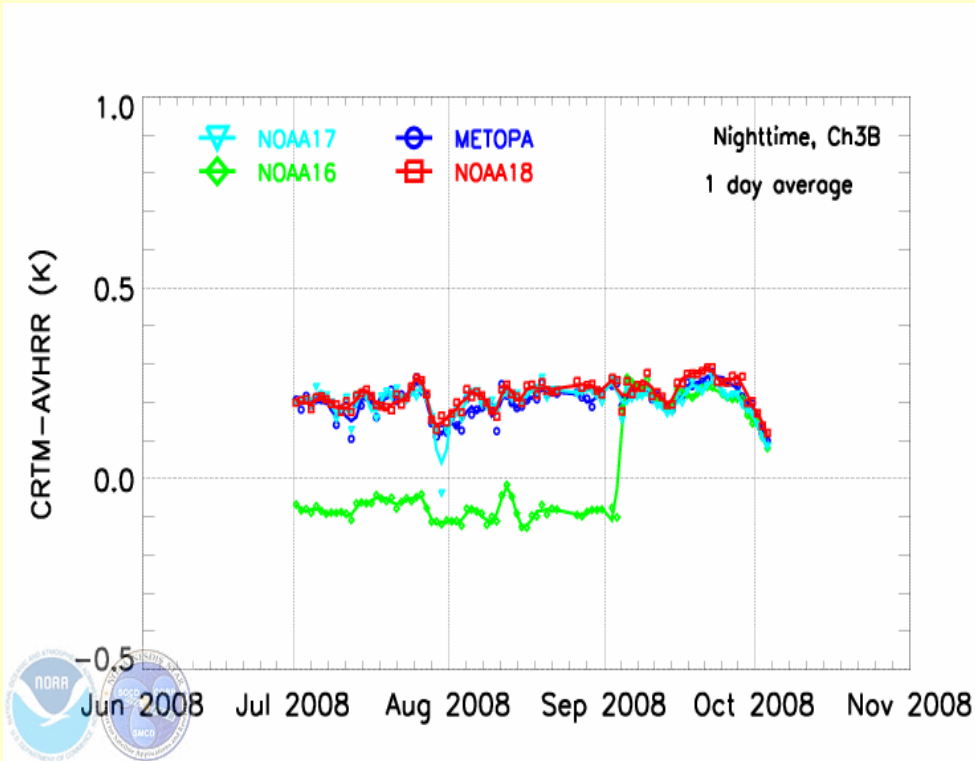




# Paul vanDelst at Party



# Collaboration: User -- CRTM -- Sensor

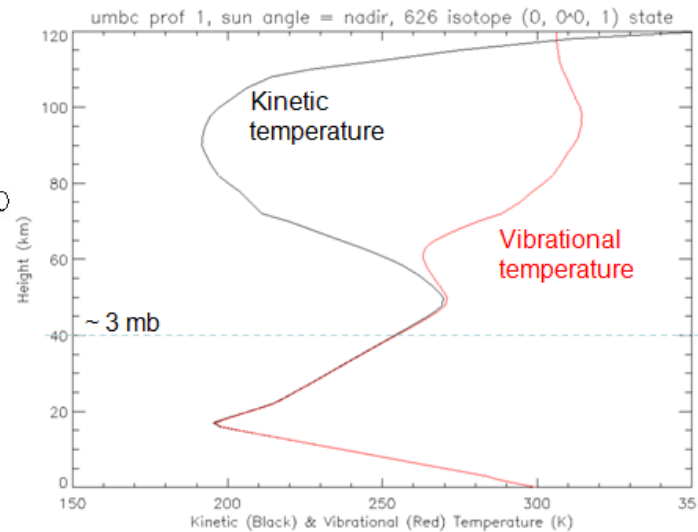
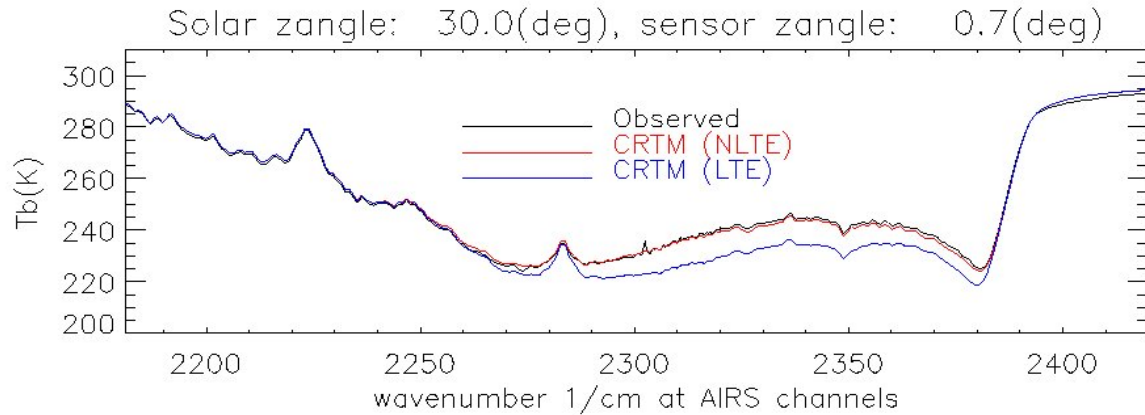
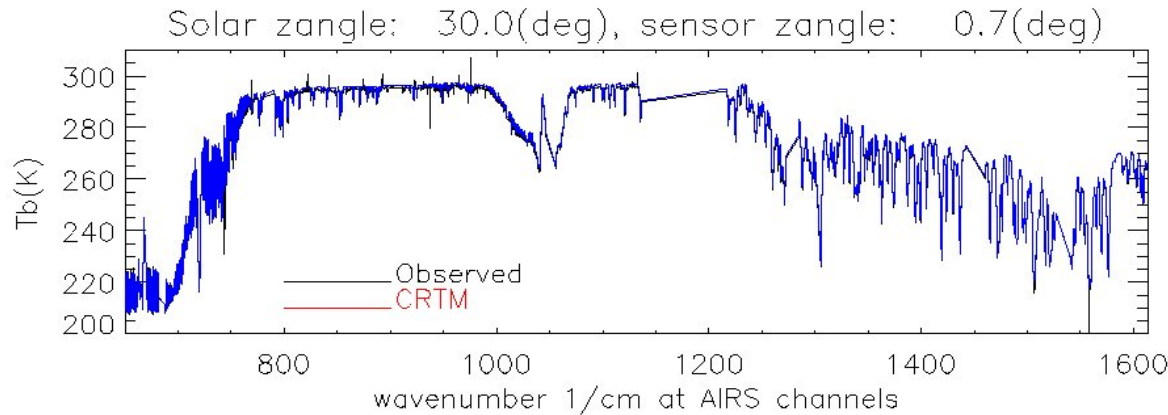


The black line is the transmittance between 0.005 (model top) and 20 hPa.

User reported an unexpected bias ( $B - O$ ) for NOAA-16 Ch. 3b. CRTM team found that out-of-band was the root cause, and the sensor team confirmed the cause.

# CRTM NLTE Simulation vs Observation, Solar zenith angle = 30°, Sensor zenith angle = 0.7°

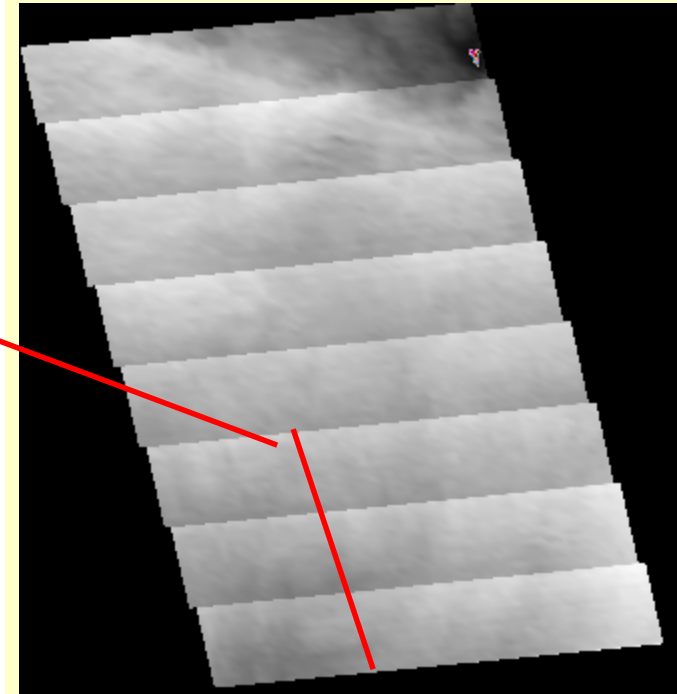
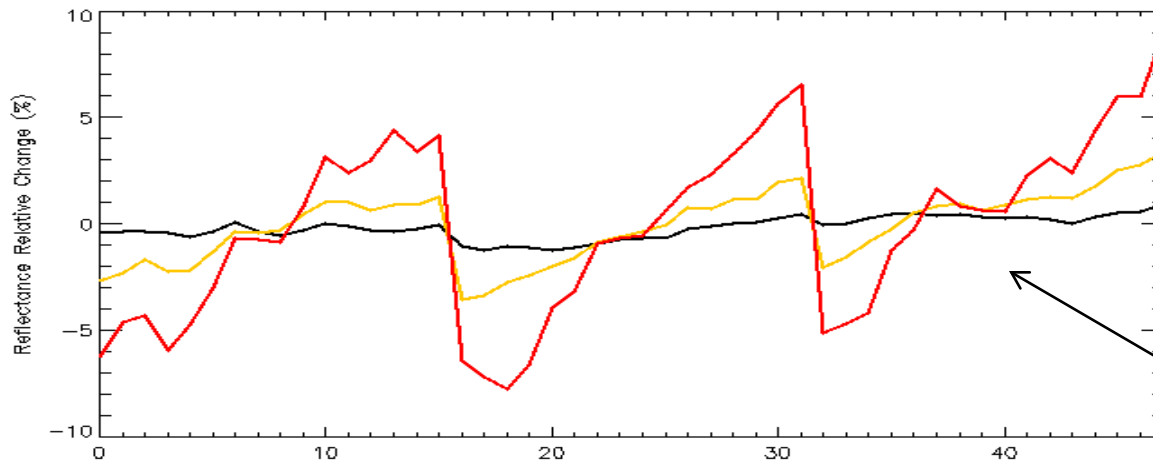
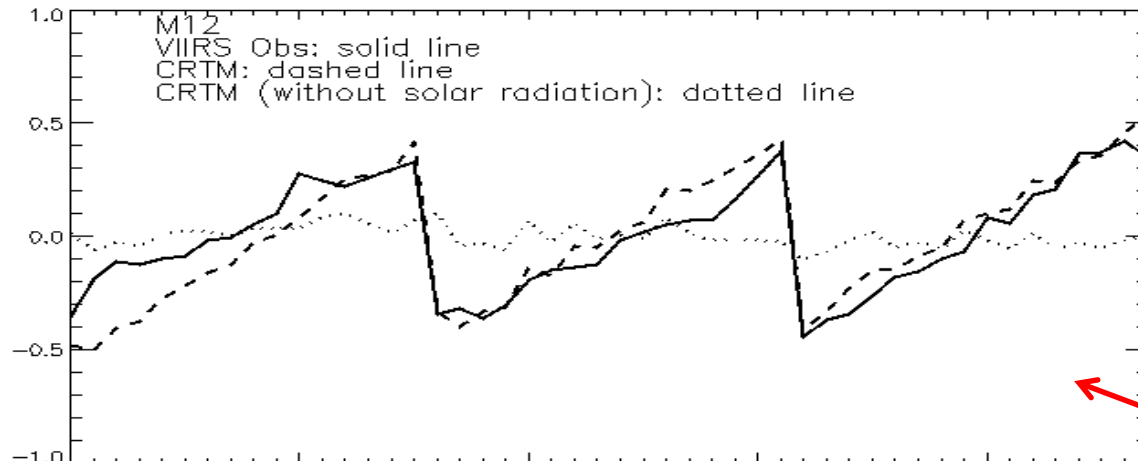
AIRS



$$\Delta R_{ch}(\theta^{sen}, \theta^{sun}) = c_0(\theta^{sen}, \theta^{sun}) + c_1(\theta^{sen}, \theta^{sun})T_{m1} + c_2(\theta^{sen}, \theta^{sun})T_{m2}$$

$$T_{m1} (0.005-0.2\text{hPa}), T_{m2} (0.2-52\text{hPa}) \quad 7$$

# VIIRS and CRTM Modeling for M12 Striping Investigation



M1, M4, and M11 measured  $(R-R_m)/R_m * 100$

The STAR team applied the CRTM to simulate the VIIRS SDR data. It is found that the M12 striping reported by the SST EDR team is caused by the difference in VIIRS azimuth angles among detectors.



# Detailed CRTM Calculation for the Striping

| Detector # | $\tau(\theta_{sat})$ | $\phi_{sat}$ | BRDF    | A       | B       | R       | Brightness temperature |
|------------|----------------------|--------------|---------|---------|---------|---------|------------------------|
| 1          | 0.73685              | 80.368       | 0.04253 | 0.51055 | 0.10590 | 0.61645 | 302.666                |
| 2          | 0.73649              | 80.543       | 0.04309 | 0.50923 | 0.10717 | 0.61641 | 302.648                |
| 3          | 0.73700              | 80.717       | 0.04365 | 0.51022 | 0.10873 | 0.61894 | 302.738                |
| 4          | 0.73645              | 80.892       | 0.04422 | 0.50964 | 0.10999 | 0.61962 | 302.769                |
| 5          | 0.73705              | 81.066       | 0.04479 | 0.51114 | 0.11159 | 0.62273 | 302.871                |
| 6          | 0.73628              | 81.241       | 0.04537 | 0.51147 | 0.11280 | 0.62427 | 302.931                |
| 7          | 0.73701              | 81.415       | 0.04596 | 0.51164 | 0.11448 | 0.62612 | 302.987                |
| 8          | 0.73596              | 81.589       | 0.04656 | 0.51074 | 0.11566 | 0.62640 | 303.020                |
| 9          | 0.73673              | 81.764       | 0.04715 | 0.51175 | 0.11739 | 0.62914 | 303.115                |
| 10         | 0.73557              | 81.938       | 0.04776 | 0.51124 | 0.11855 | 0.62978 | 303.153                |
| 11         | 0.73641              | 82.113       | 0.04837 | 0.51120 | 0.12036 | 0.63157 | 303.230                |
| 12         | 0.73509              | 82.287       | 0.04901 | 0.51134 | 0.12155 | 0.63289 | 303.316                |
| 13         | 0.73562              | 82.461       | 0.04962 | 0.51180 | 0.12325 | 0.63505 | 303.396                |
| 14         | 0.73486              | 82.636       | 0.05026 | 0.51057 | 0.12461 | 0.63518 | 303.417                |
| 15         | 0.73526              | 82.810       | 0.05089 | 0.50993 | 0.12629 | 0.63622 | 303.439                |
| 16         | 0.73565              | 82.985       | 0.05154 | 0.50998 | 0.12812 | 0.63810 | 303.560                |

$$R = \tau(\theta_{sat})[\varepsilon B(T_s) + (1 - \varepsilon)R_{atm\_d}] + R_{atm\_u} + F_0 \cos(\theta_{sun}) \tau(\theta_{sun}) BRDF(\theta_{sun}, \theta_{sat}, \phi_{sun} - \phi_{sat}) \tau(\theta_{sat})$$

A

B

# Microwave Integrated Retrieval System (MiRS)

- Cost Function to minimize:

$$J(\mathbf{X}) = \left[ \frac{1}{2} \underbrace{(\mathbf{X} - \mathbf{X}_0)^T \times \mathbf{B}^{-1} \times (\mathbf{X} - \mathbf{X}_0)}_{\text{Bkg-departure normalized by Bkg Error}} \right] + \left[ \frac{1}{2} \underbrace{(\mathbf{Y}^m - \mathbf{Y}(\mathbf{X}))^T \times \mathbf{E}^{-1} \times (\mathbf{Y}^m - \mathbf{Y}(\mathbf{X}))}_{\text{Measurements-departure normalized by Measurements+Modeling Errors}} \right]$$

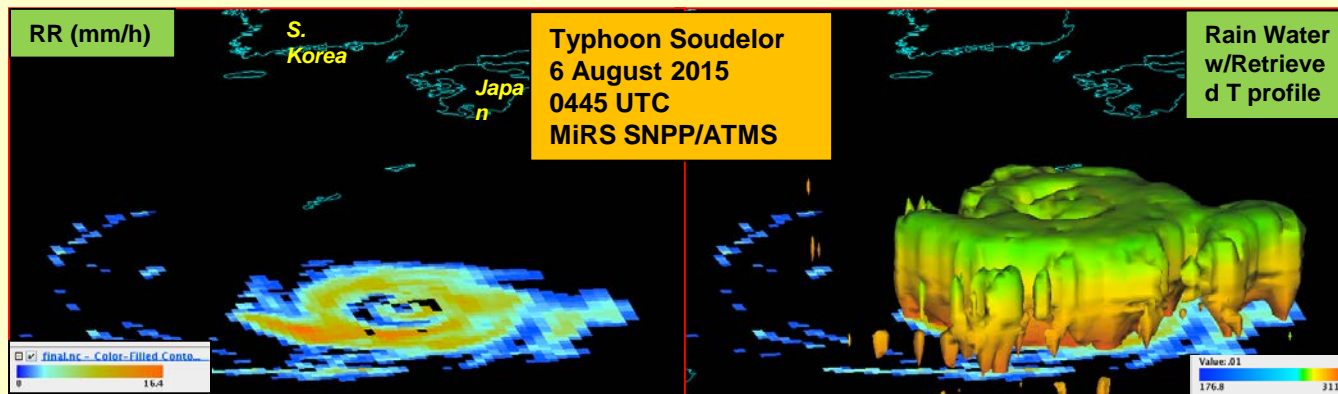
Previously updated in V11

- To find the optimal solution, solve for:  $\frac{\partial J(\mathbf{X})}{\partial \mathbf{X}} = \mathbf{J}'(\mathbf{X}) = 0$
- Assuming local Linearity:  $y(\mathbf{x}) = y(\mathbf{x}_0) + \mathbf{K}[\mathbf{x} - \mathbf{x}_0]$
- This leads to iterative solution:

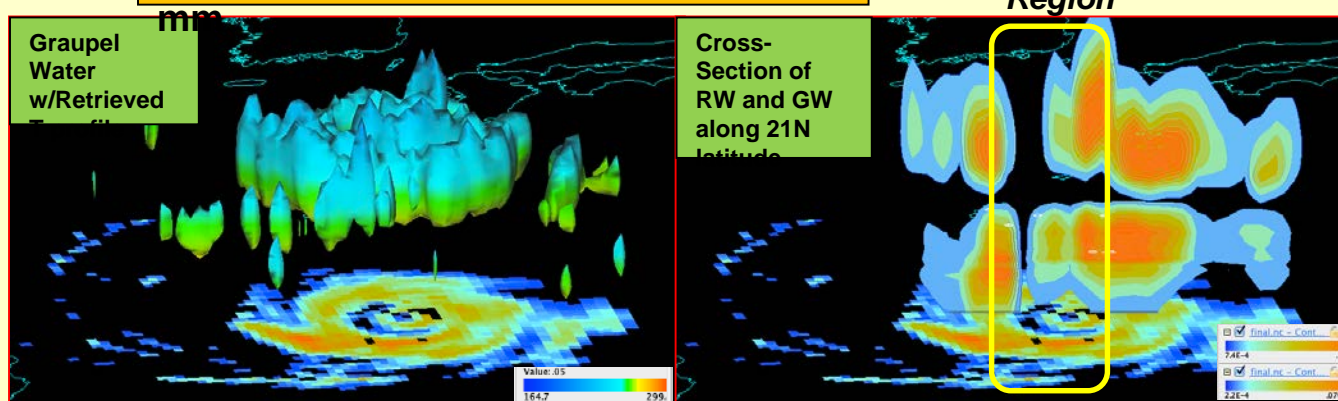
$$\Delta \mathbf{X}_{n+1} = \left\{ \mathbf{B} \mathbf{K}_n^T (\mathbf{K}_n \mathbf{B} \mathbf{K}_n^T + \mathbf{E})^{-1} \right\} [(\mathbf{Y}^m - \mathbf{Y}(\mathbf{X}_n)) + \mathbf{K}_n \Delta \mathbf{X}_n]$$

# Typhoon Soudelor 3-Dimensional Structure

- MiRS simultaneous retrieval of temperature profile and hydrometeors allows depiction of storm structure

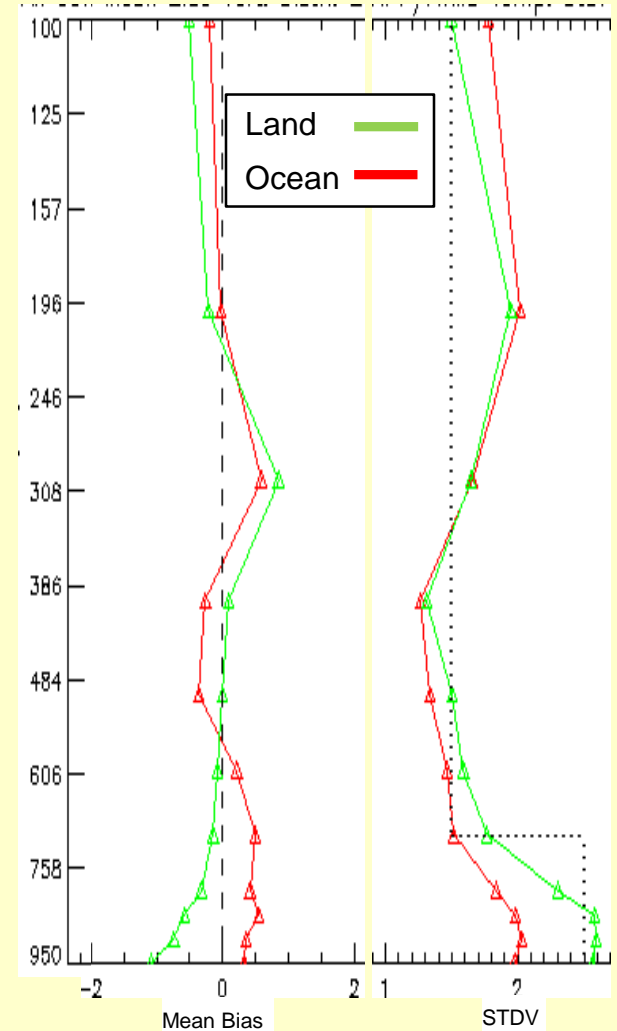
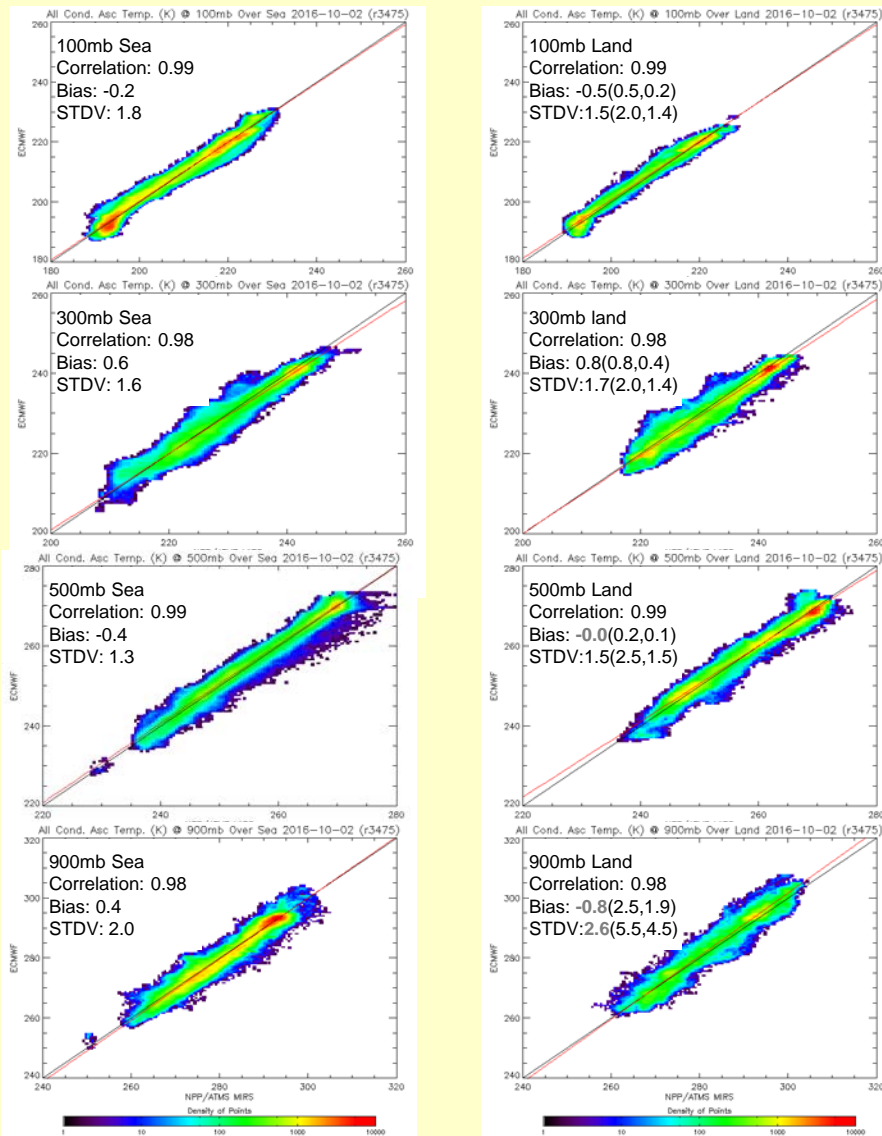


Isosurfaces: GW=0.05 mm, RW=0.01



# Validation Results: Temperature Profile

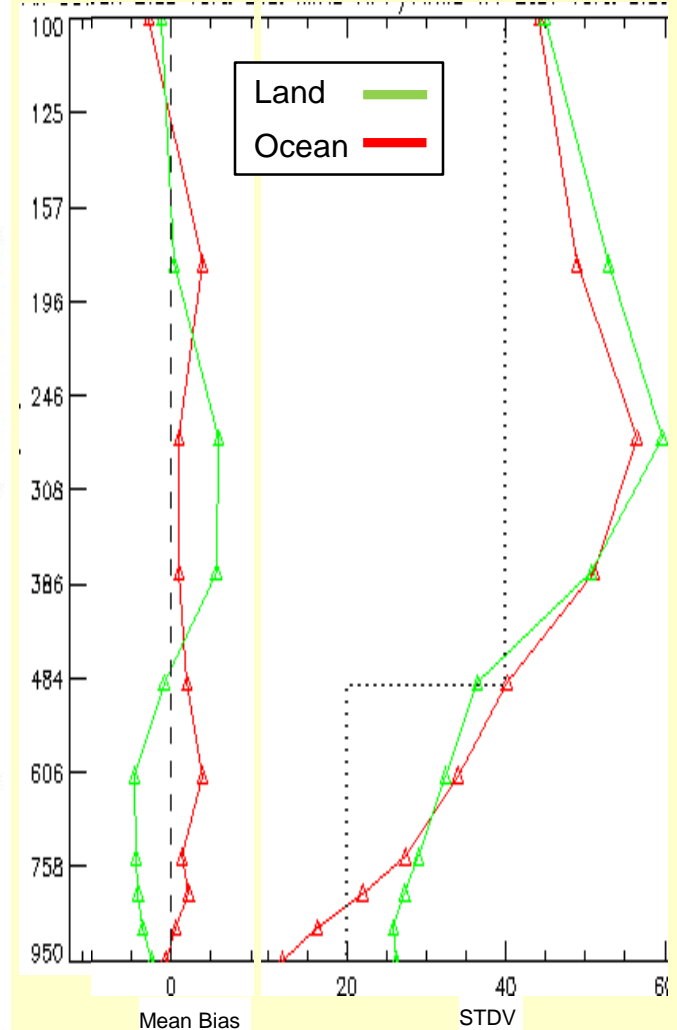
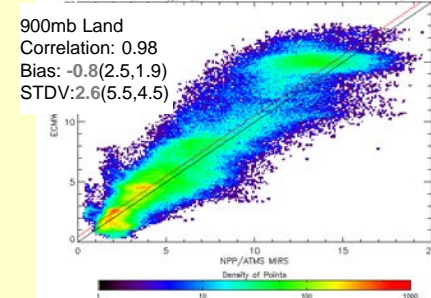
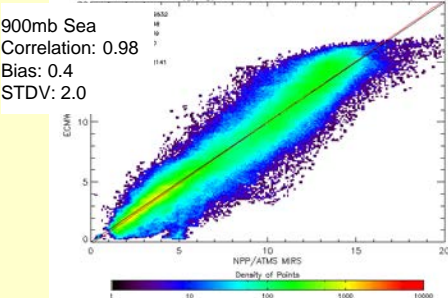
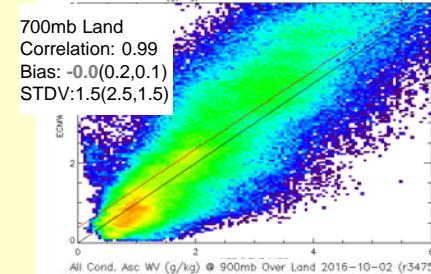
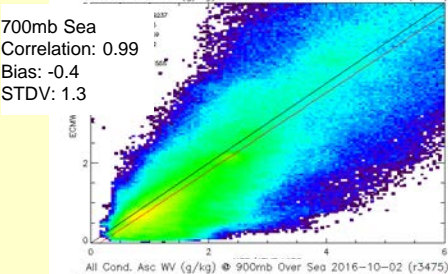
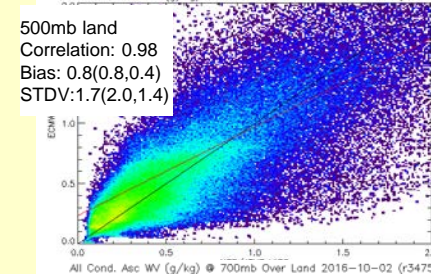
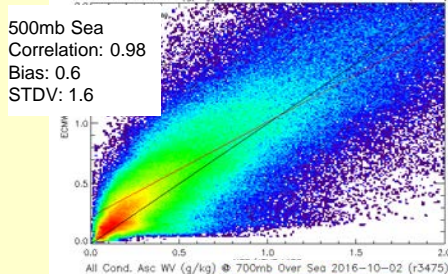
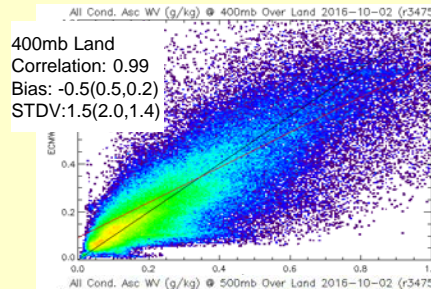
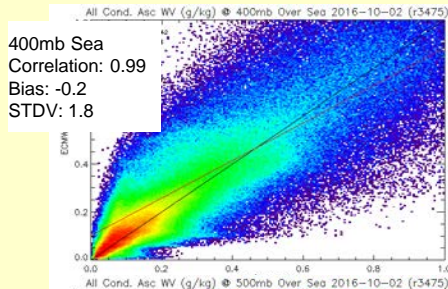
Global all Condition T Statistic refer to ECMWF



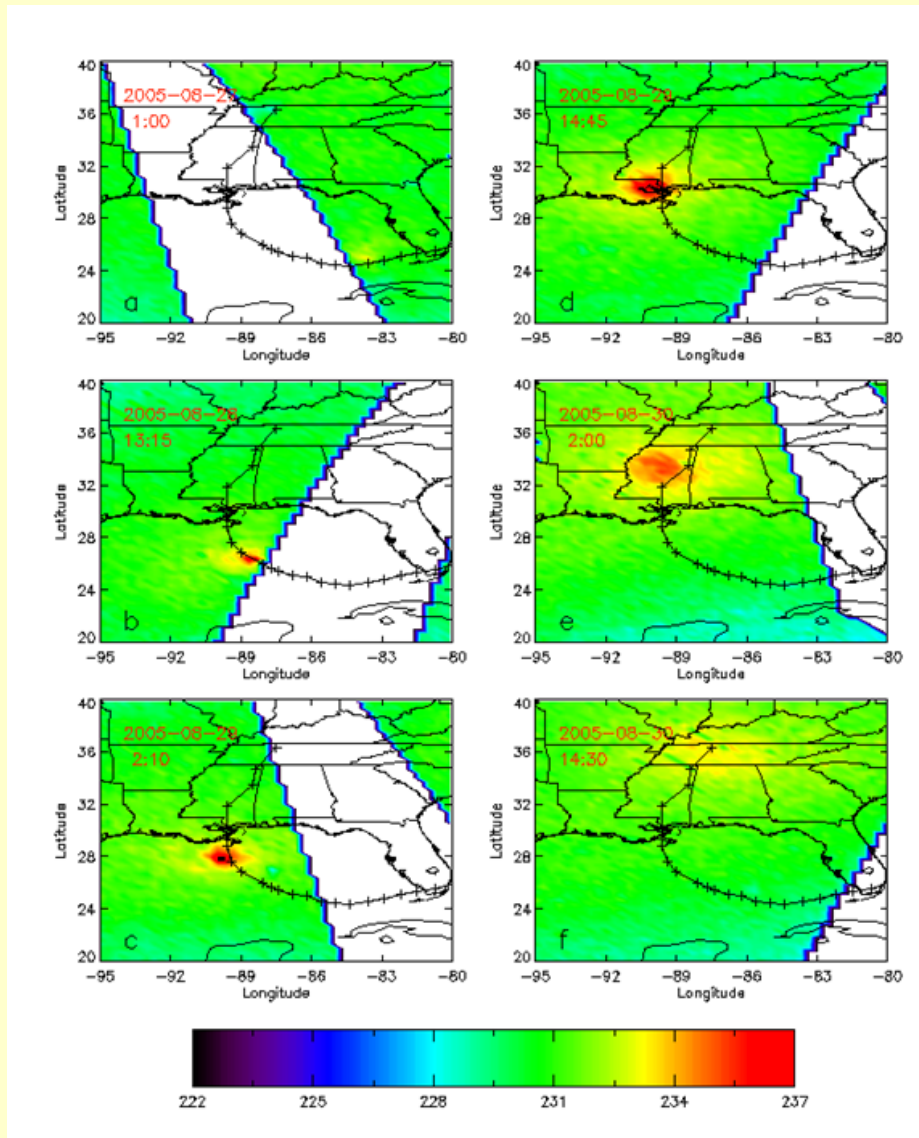


# Validation Results: Water Vapor Profile

Global all Condition Water Vapor Statistic refer to ECMWF



# Radiances in studying Hurricane (warm Core from SSMIS Observations at 54.4 GHz)



The SSMIS measures radiances in 24 channels covering a wide range of frequencies (19 – 183 GHz) conical scan geometry at an earth incidence angle of 53 degrees maintains uniform spatial resolution, across the entire swath of 1700 km.

# Comparison between Test-run and Control-run

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| Forecasting time (hour) | Surface minimum pressure (hPa) |        |             | Surface maximum wind (m/s) |       |             |
|-------------------------|--------------------------------|--------|-------------|----------------------------|-------|-------------|
|                         | Control                        | Test   | Observation | Control                    | Test  | Observation |
| 00                      | 988.87                         | 983.31 | 959.00      | 26.18                      | 31.51 | 46.20       |
| 06                      | 981.55                         | 974.60 | 950.00      | 36.36                      | 30.46 | 48.80       |
| 12                      | 970.80                         | 957.90 | 942.00      | 39.05                      | 39.33 | 51.40       |
| 18                      | 964.45                         | 945.81 | 948.00      | 39.97                      | 48.99 | 51.40       |
| 24                      | 951.71                         | 936.11 | 941.00      | 45.19                      | 49.31 | 51.40       |
| 30                      | 935.58                         | 923.40 | 930.00      | 49.40                      | 57.20 | 64.20       |
| 36                      | 927.75                         | 913.17 | 909.00      | 54.86                      | 58.20 | 74.50       |
| 42                      | 918.92                         | 908.72 | 902.00      | 57.94                      | 58.31 | 77.10       |
| 48                      | 916.38                         | 905.25 | 905.00      | 54.31                      | 59.67 | 71.90       |

Control: operational at that time

Test: Control + SSMIS

# Discussions

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- Satellite sensor data assimilations for NWP and data assimilation at the STAR
- Radiometric data impact assessment in Observing System Simulation Experiments (OSSEs)
- Radiometric instrument design, calibration and monitoring (e.g. ICVS)
- Physical retrievals of atmospheric and surface state variables (JPSS MiRS, GOES-R sounding)
- Air-quality monitoring and forecast
- Reanalysis and climate studies
- Aircraft campaign
- SmallSat and CubeSat innovation (e.g. MicroMas-2)
- Scientific research and education