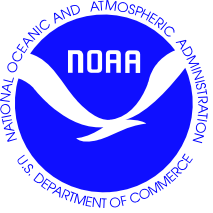




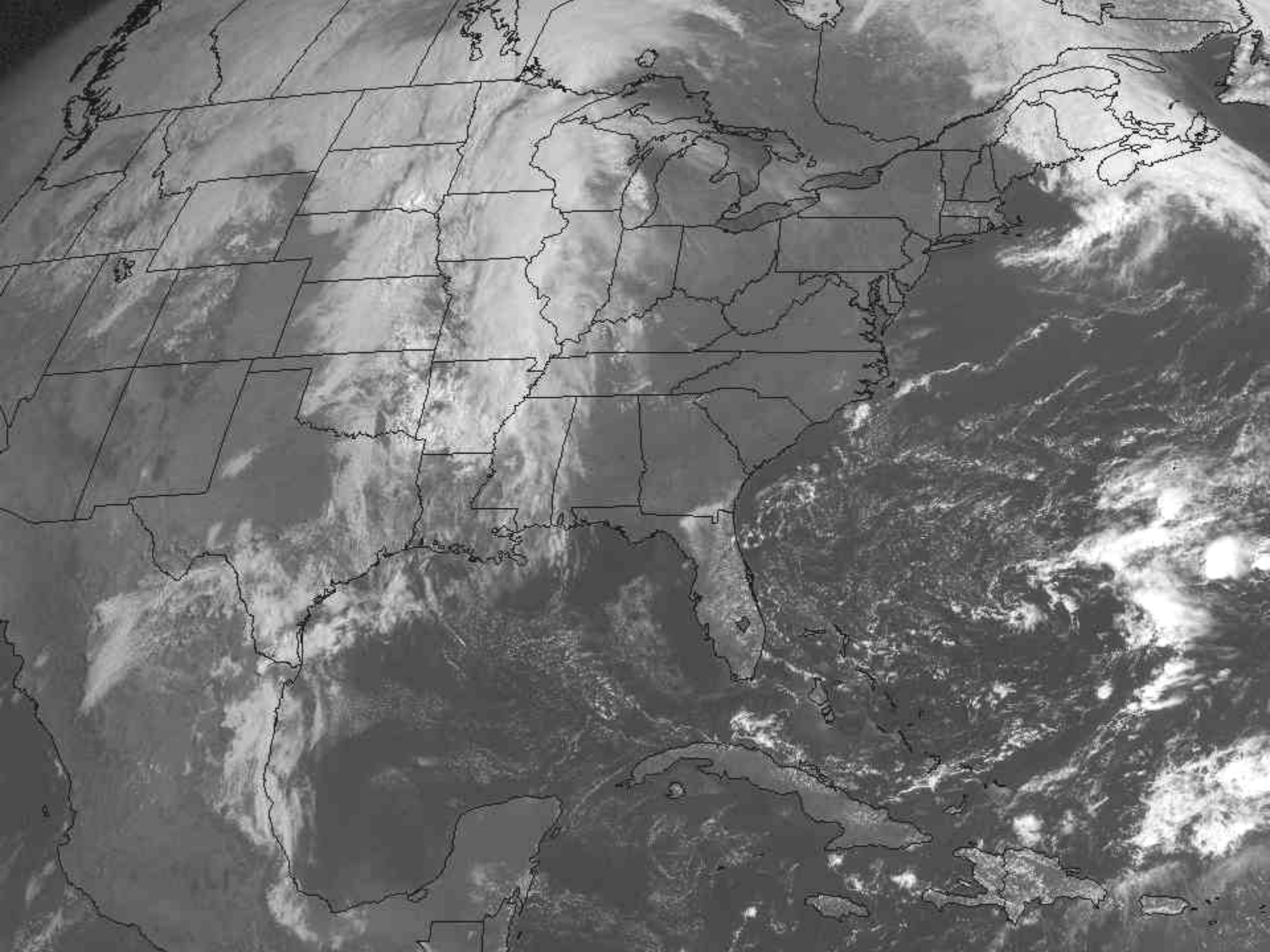
Microwave Radiative Transfer at the Sub-Field-of-View Resolution

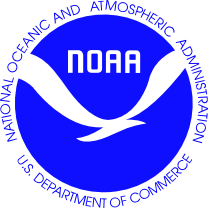
Thomas J. Kleespies
NOAA/NESDIS



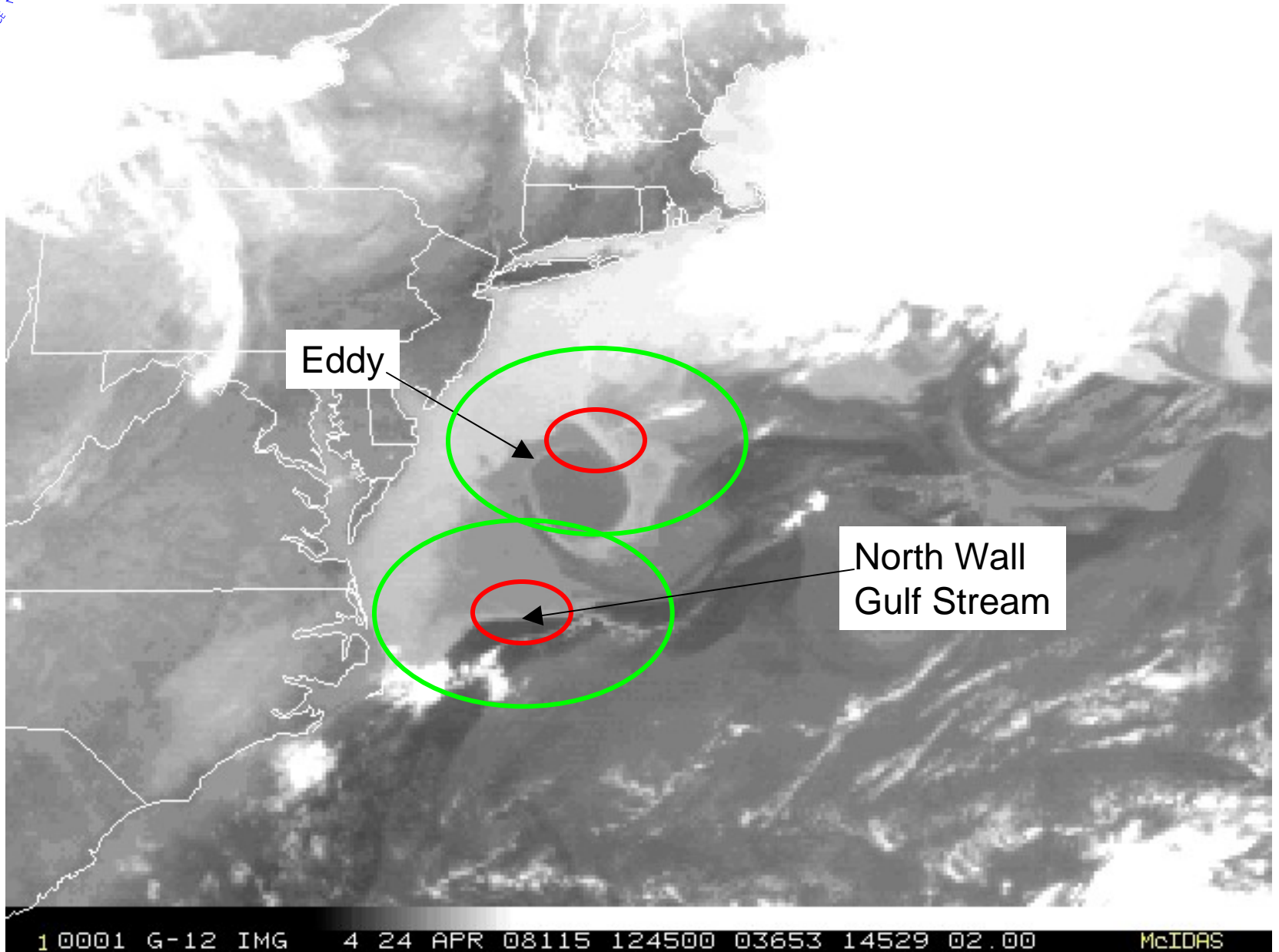
Problem

- Radiative transfer with channels that ‘see’ the surface is problematic because of emissivity and skin temperature uncertainties
- This is especially true of inhomogeneous backgrounds, including coastlines, large rivers, mountainous regions, and even regions of high ocean temperature gradients (e.g. north wall of Gulf Stream).





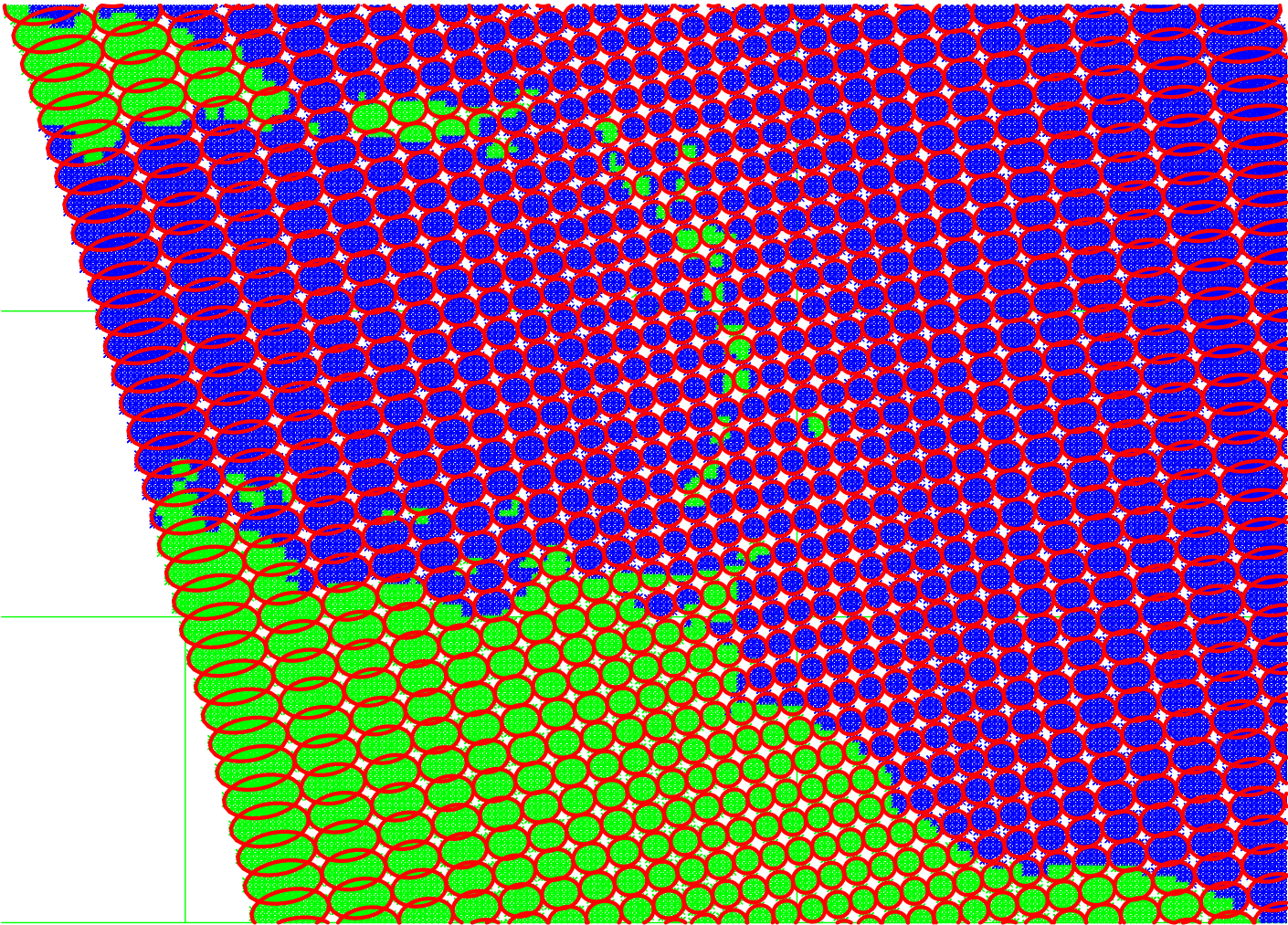
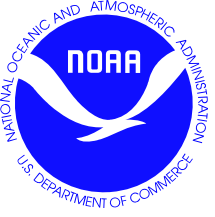
Inhomogeneous surface over ocean

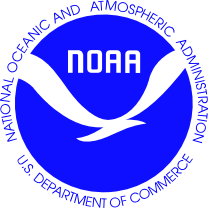




Possible Solution

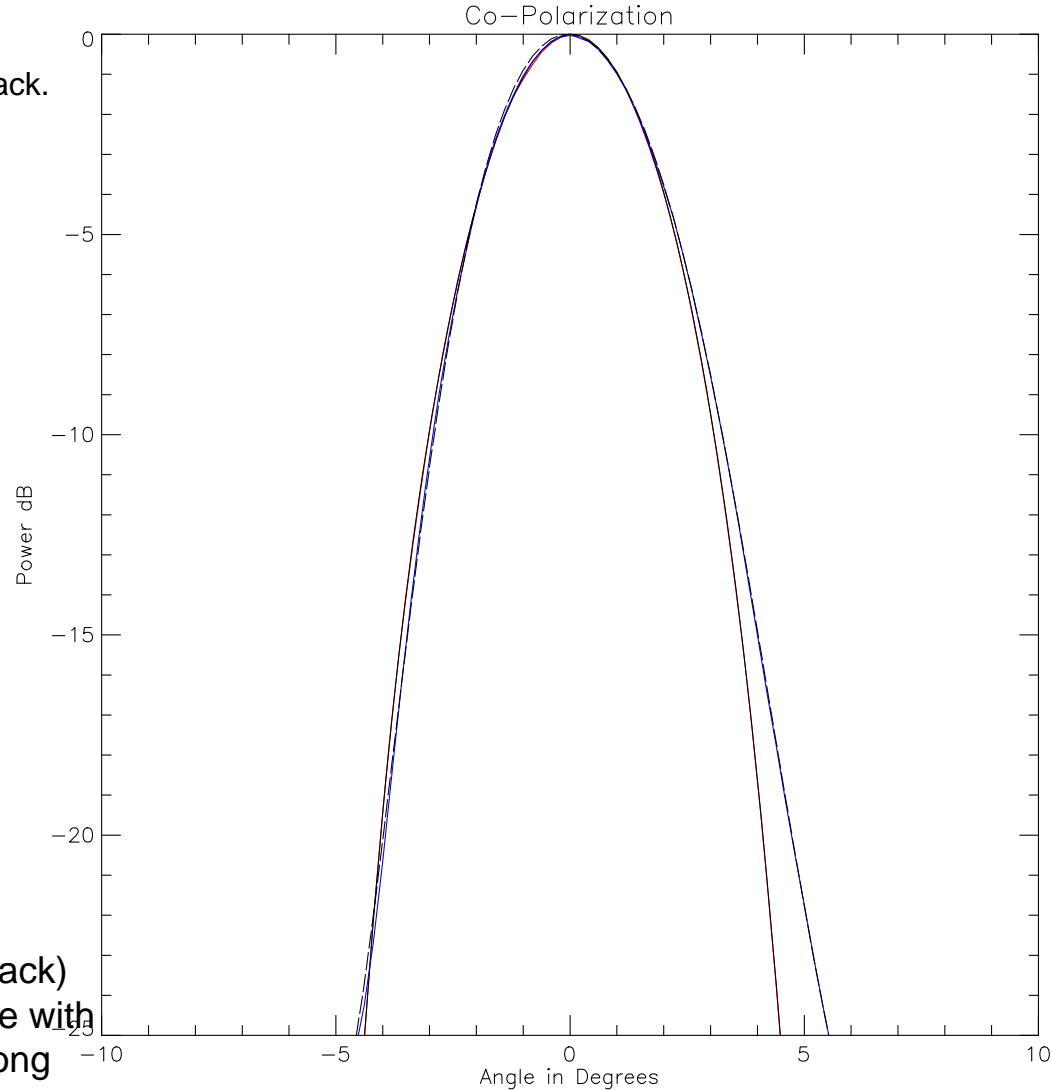
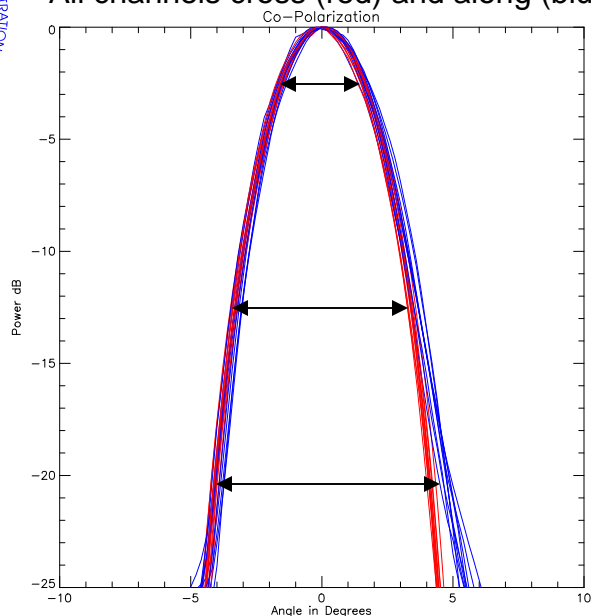
- The ability to integrate high resolution databases within a given field-of-view, and perform multiple radiative transfer within the field of view, weigh that according to the antenna beam power, and integrate.





METOP AMSUA

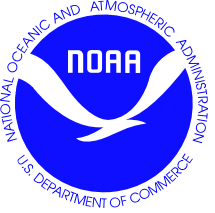
All channels cross (red) and along (blue) track.



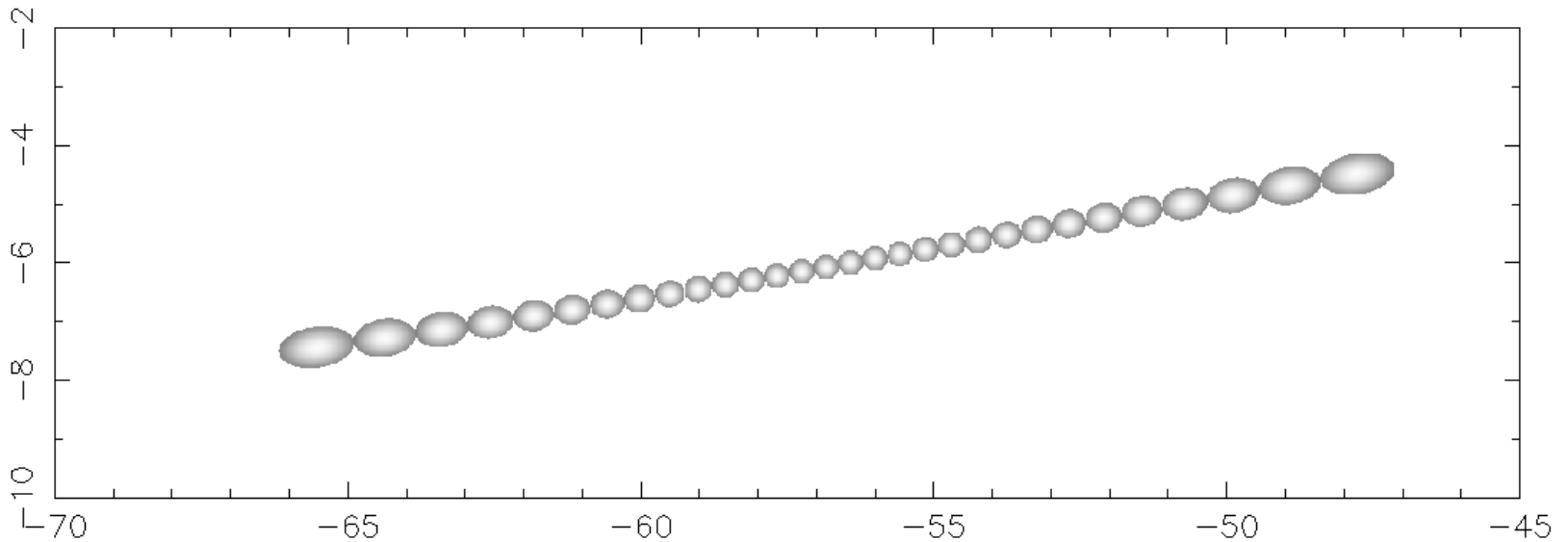
Normalized antenna patterns by adding (negative) maximum value of each pattern to all values. Averaged all 10 channels for the 0 deg (red-crosstrack) and 90 deg (blue alongtrack). Got best fit to the eye with a 7th order polynomial (solid, crosstrack, dashed along track).

99% power inside the fov is at -20 dB. This is approx 10 deg wide. Ran this through the fov_angle_sizes code, compared with 3.3 deg for AMSU and got an expansion factor of 3.0 .

The solid fit line fits almost exactly over the data. The dashed fit line is almost as good.

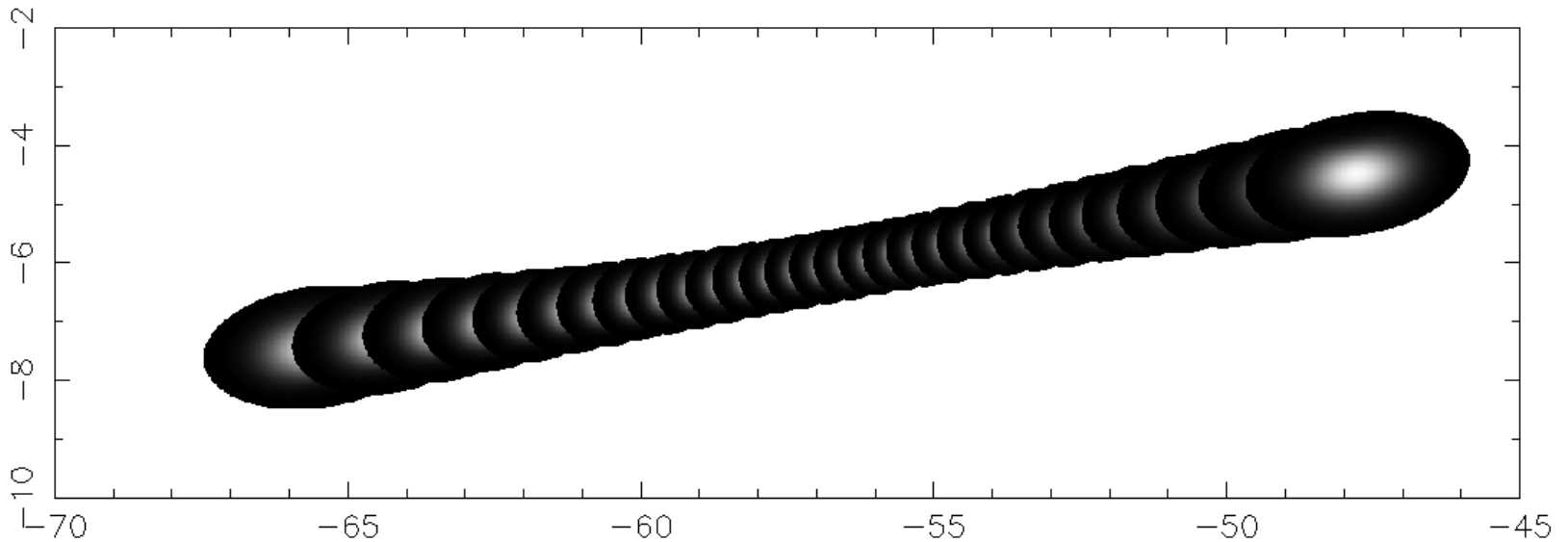


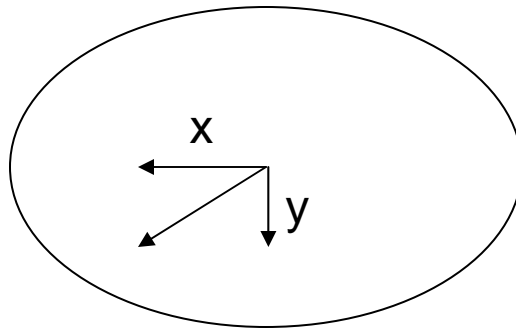
Sample AMSU scan line with relative antenna power to 50%.





Sample AMSU scan line with relative antenna power to 99%.





50% power has a dB reduction of $-10 \log_{10} .50 = -3.01$ 3.3 deg $m=1.0$

95% power has a dB reduction of $-10 \log_{10} .05 = -13.01$ 6.6 deg $m=2.0$

99% power has a dB reduction of $-10 \log_{10} .01 = -20.00$ 10.0 deg $m=3.0$

$$P_x = C_0 + \sum_{i=1}^7 C_i x^i$$

Along track power

$$P_y = D_0 + \sum_{i=1}^7 D_i y^i$$

Cross track power

$$P = -(P_x + P_y)$$

Total power

$$P_r = 10^{-P/10}$$

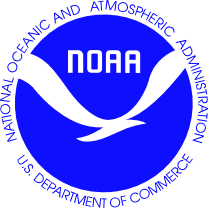
Power expressed as fraction of full power

Right now ignoring the 45° and 135° slices



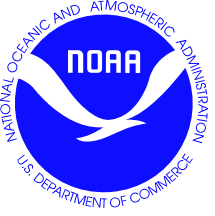
Digital Elevation Model for this Study

- GTOPO30 from USGS
- 0.008333° resolution
- translates to .93km at equator



Radiative Transfer

- CRTM
- Fastem-3 ocean, NESDIS emissivity land
- GDAS 0.5 degree resolution output
- Look for GDAS land and sea points nearest to centroid
- Integrate power/land fraction over fov
- Assume land and sea skin temperature homogeneous



Radiative Transfer continued

$$\begin{aligned} T_B &= \frac{\int_A \Phi(A) T_R(A) dA}{\int_A \Phi(A) dA} & \hat{\Phi} &= \frac{1}{\int_A \Phi(A) dA} \\ &= \hat{\Phi} \int_L \Phi(L) T_R(L) dL + \hat{\Phi} \int_S \Phi(S) T_R(S) dS \\ &= T_{RL} \hat{\Phi} \int_L \Phi(L) dL + T_{RS} \hat{\Phi} \int_S \Phi(S) dS \end{aligned}$$

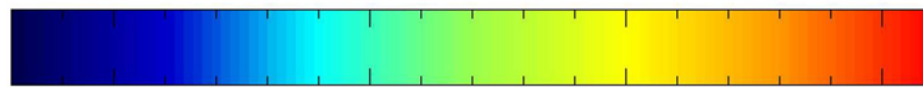
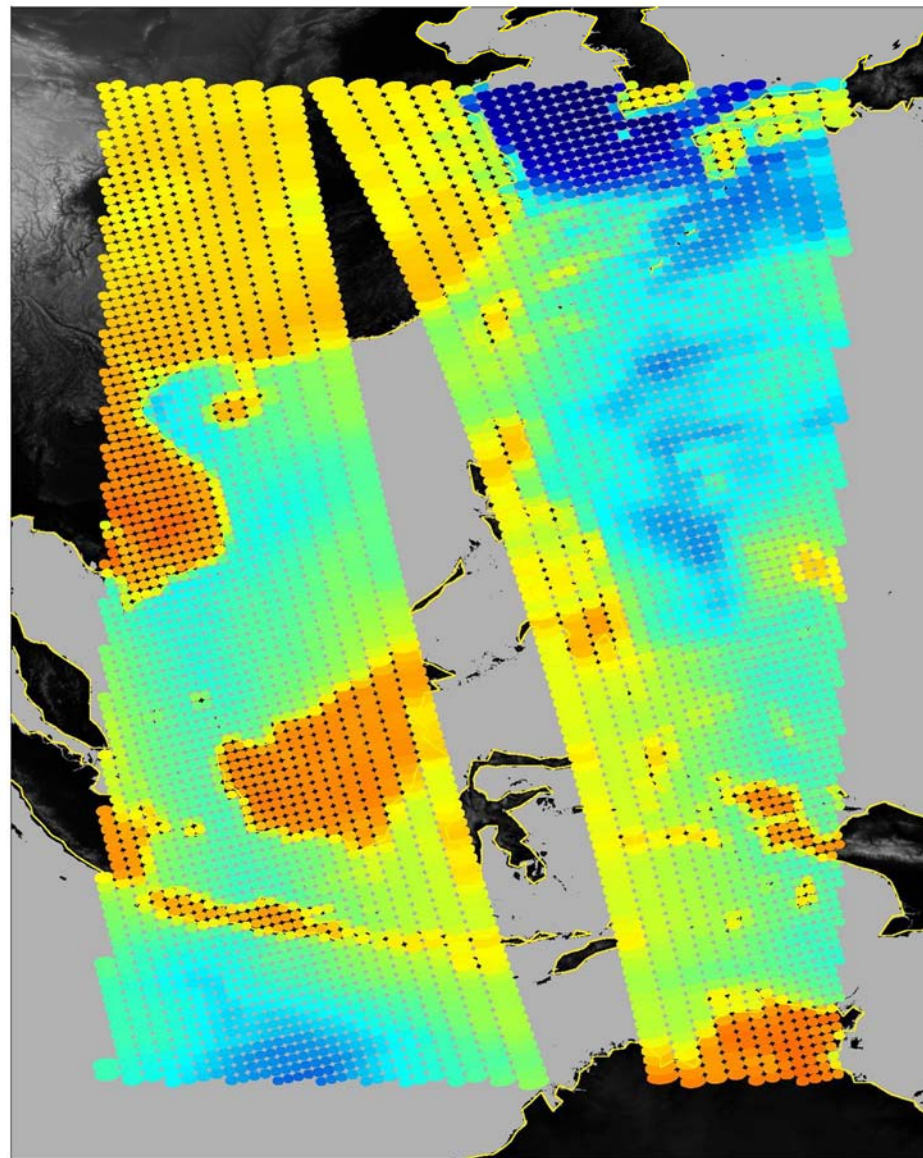
Land Power Fraction

Ocean Power Fraction

Power Fraction = Fraction of total antenna power within fov allocated to each surface type



Area of Interest



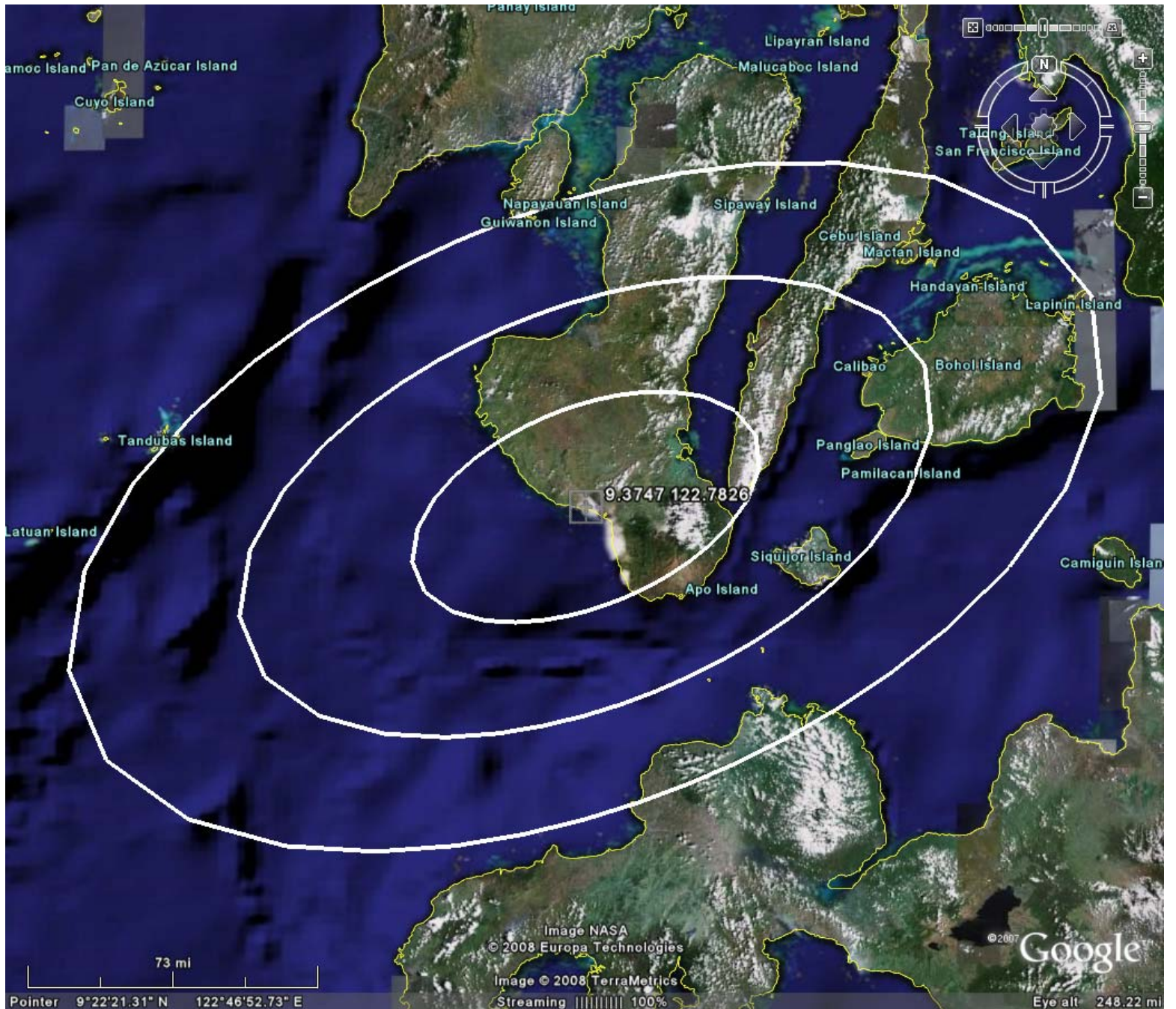
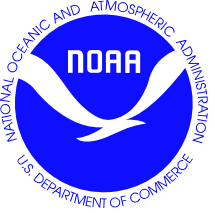
150

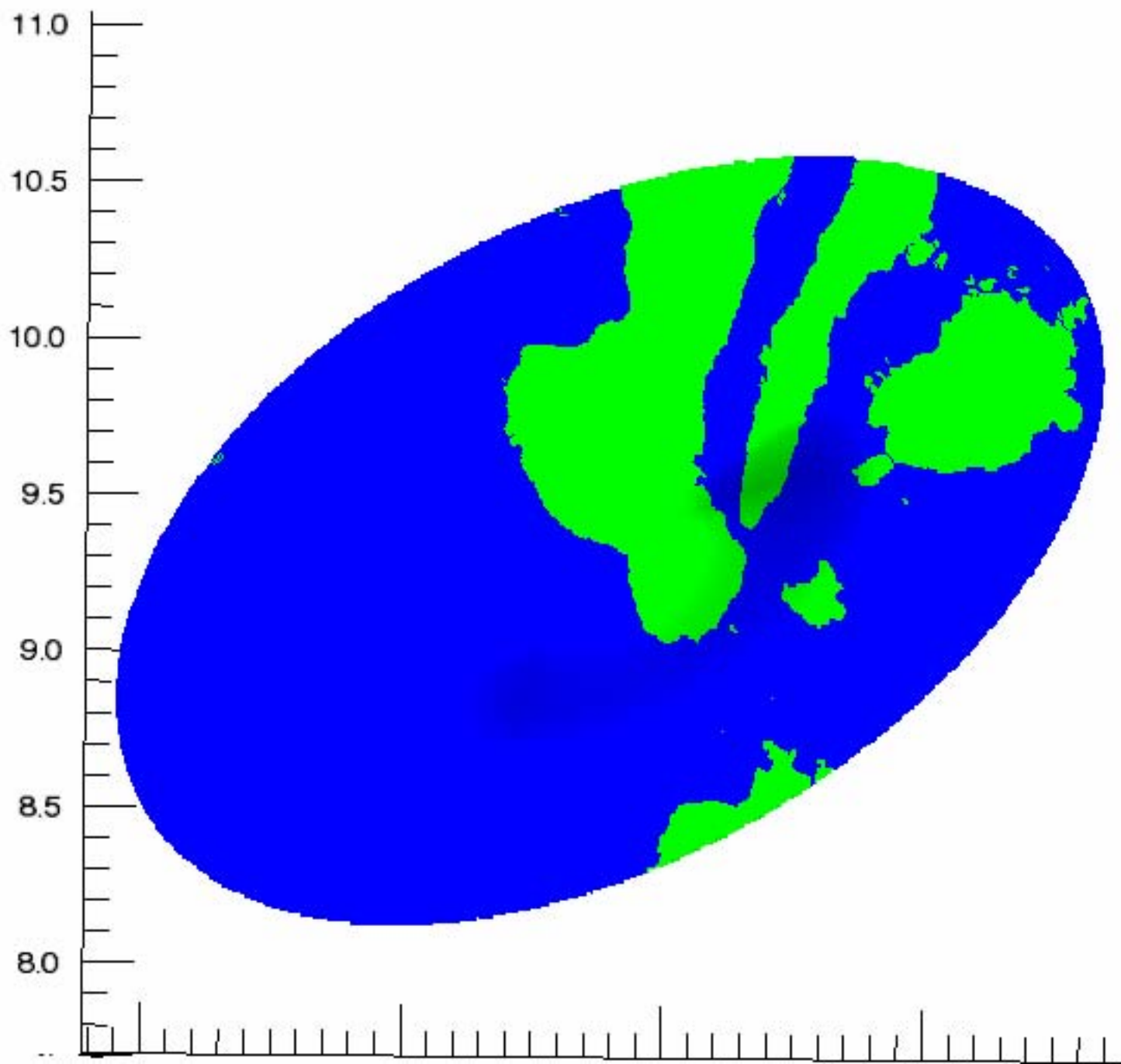
200

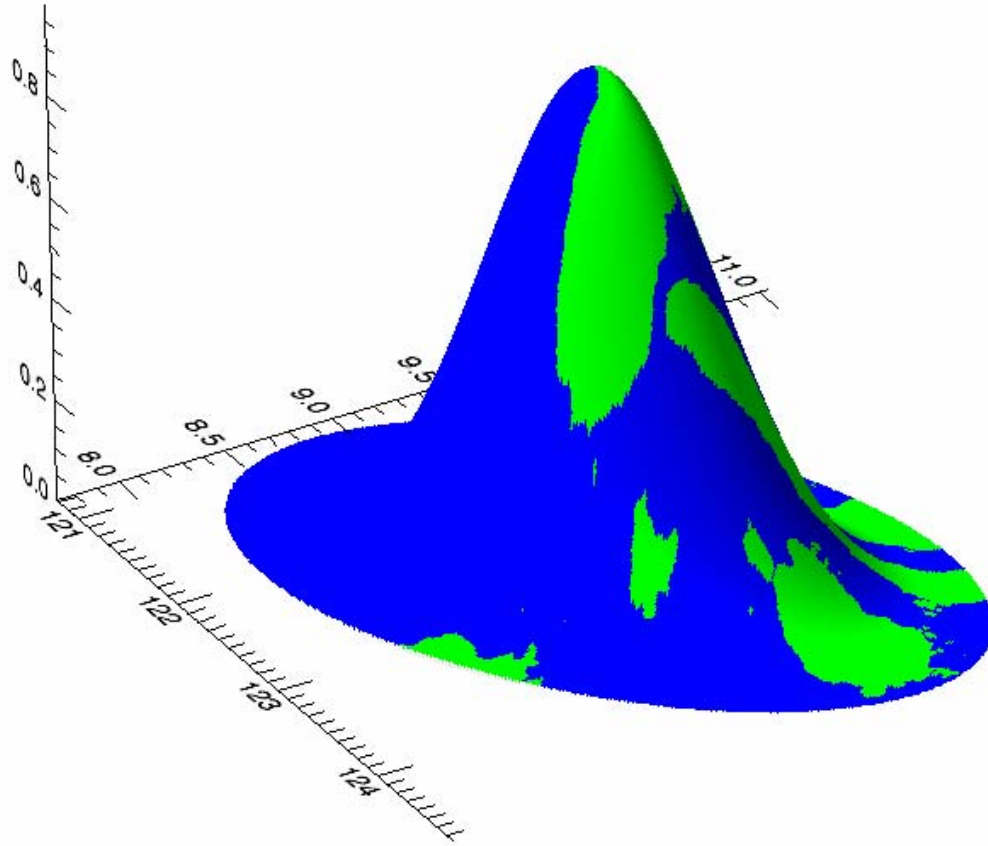
250

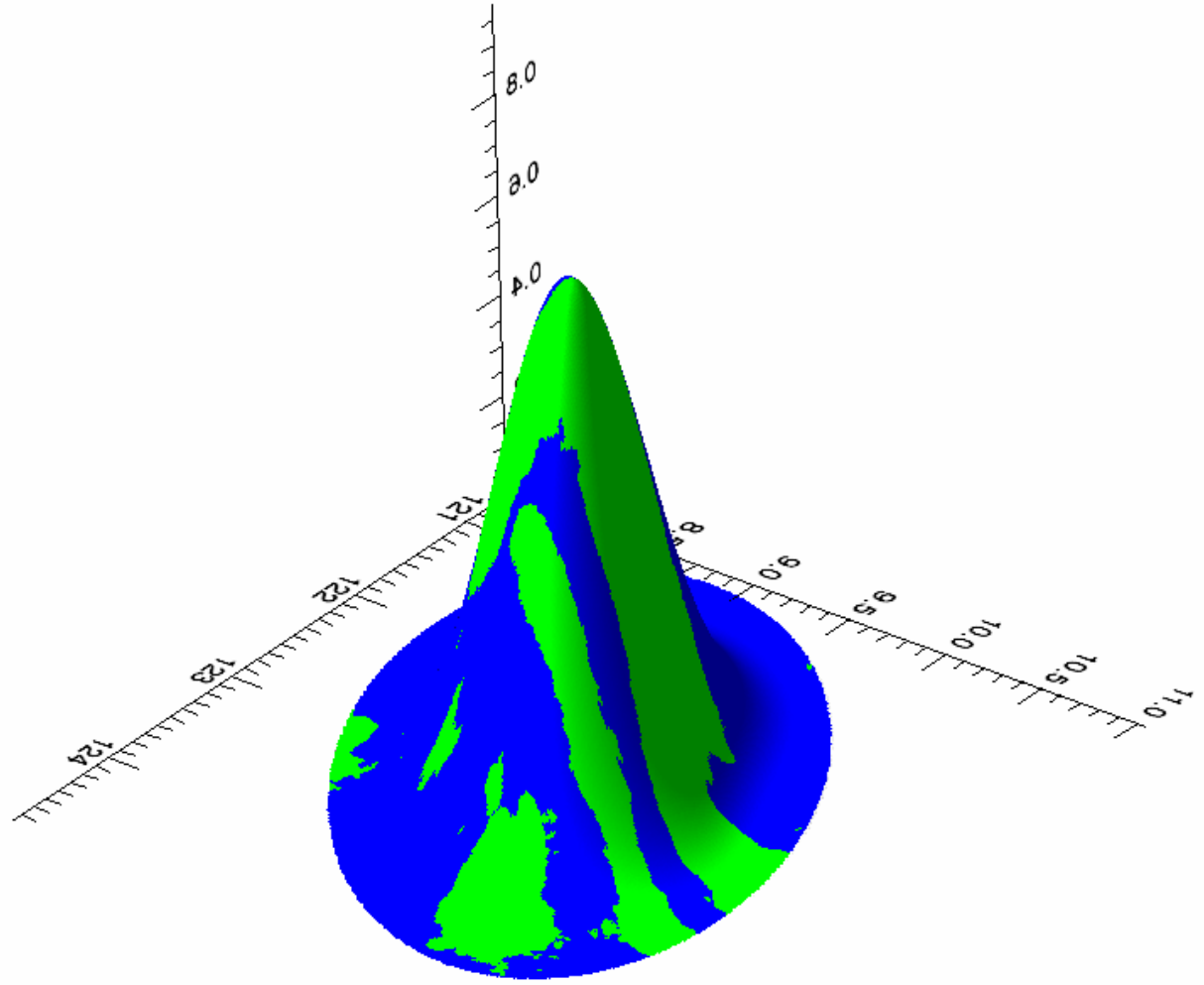
300

Brightness Temperature









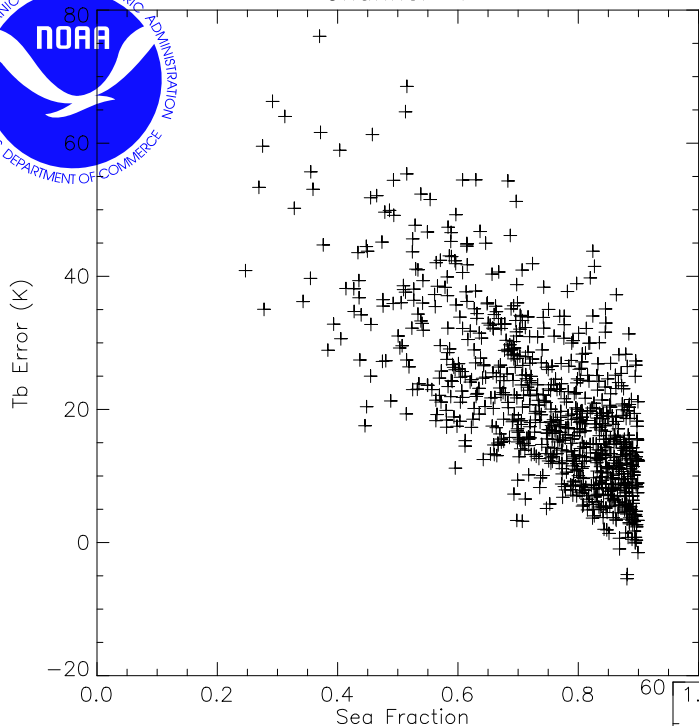
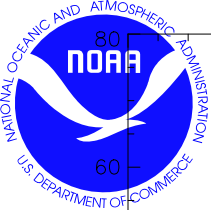


Example Tb Differences

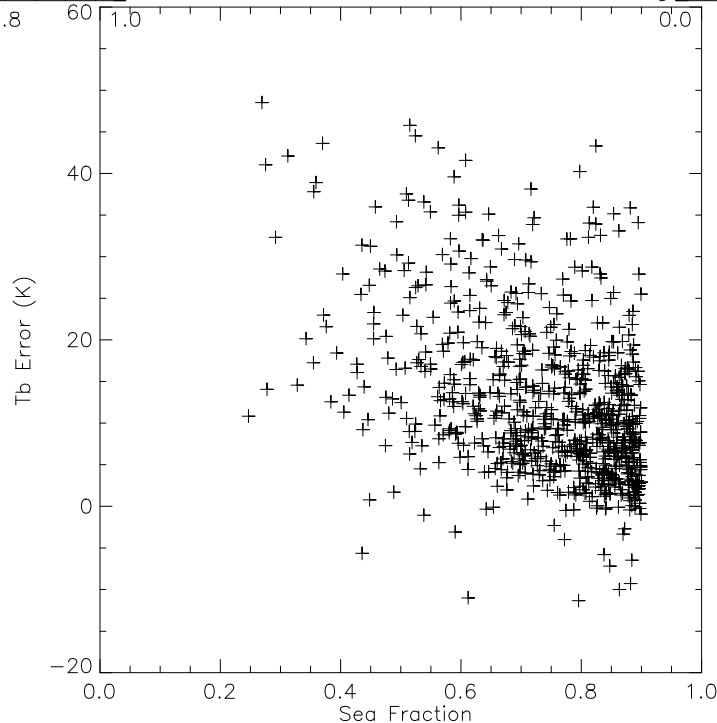
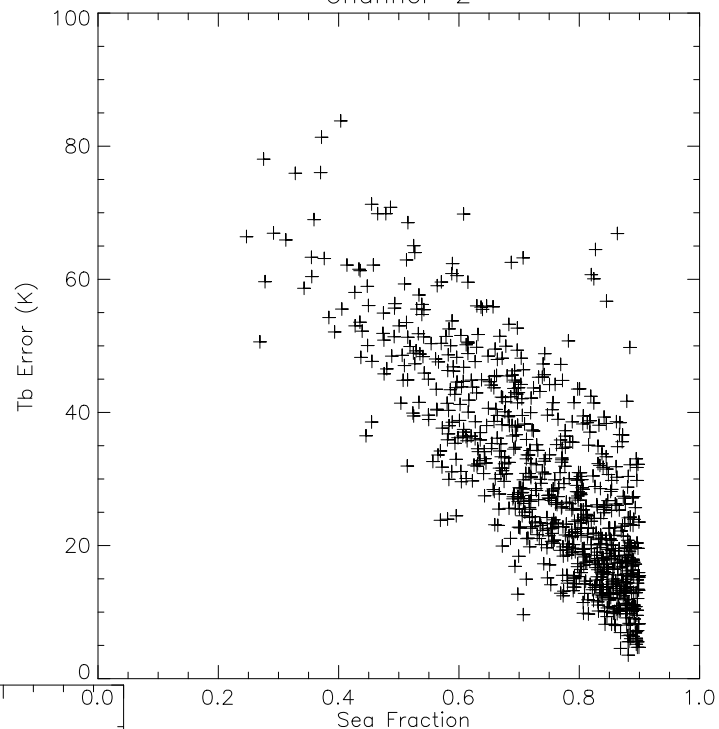
$$TB_{land} = 280 \quad TB_{sea} = 210$$

	Land Fraction	Sea Fraction	Land Power Fraction	Sea Power Fraction	Tb
99%	0.238	0.761	0.358	0.641	235.13
95%	0.301	0.698	0.371	0.628	236.01
50%	0.480	0.522	0.488	0.512	244.16

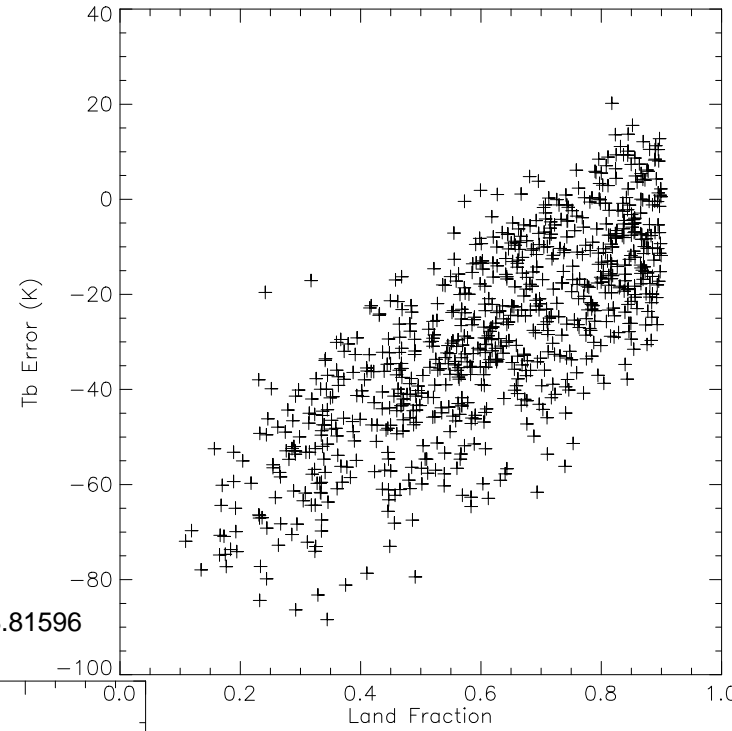
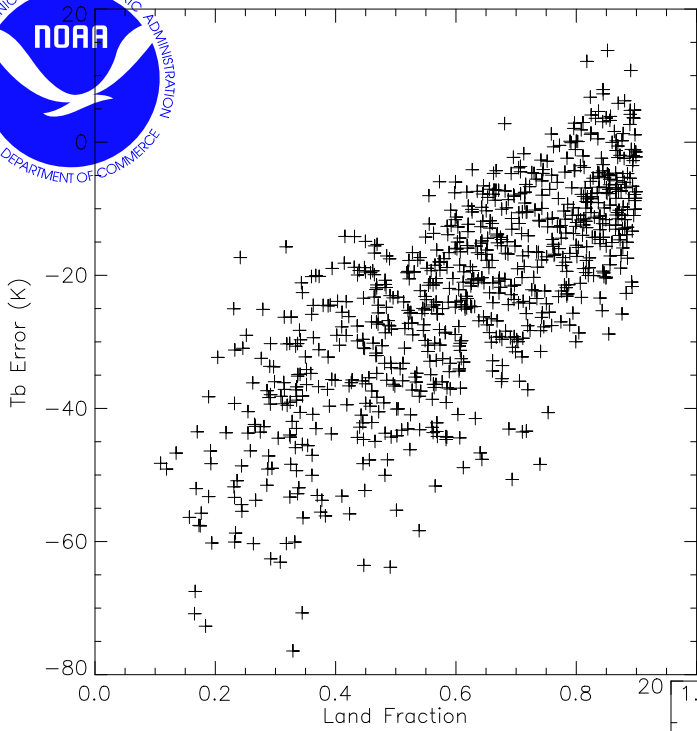
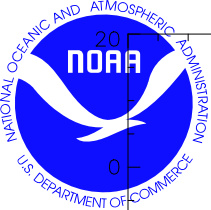
Thanks to Paul vanDelst for suggesting this comparison



Sea Mean 12.33 Stdev 9.39
Channel 15



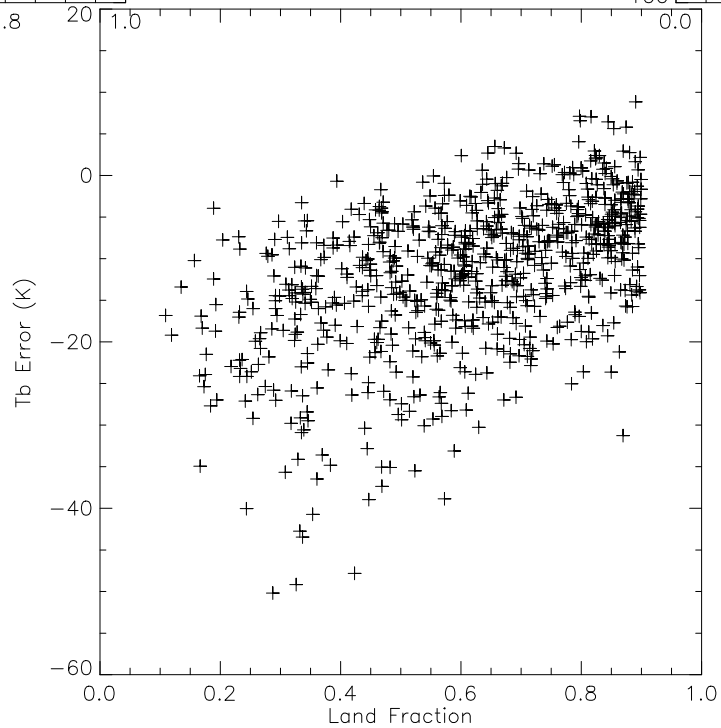
Tb Errors in coastlines
when assuming Ts is
ocean



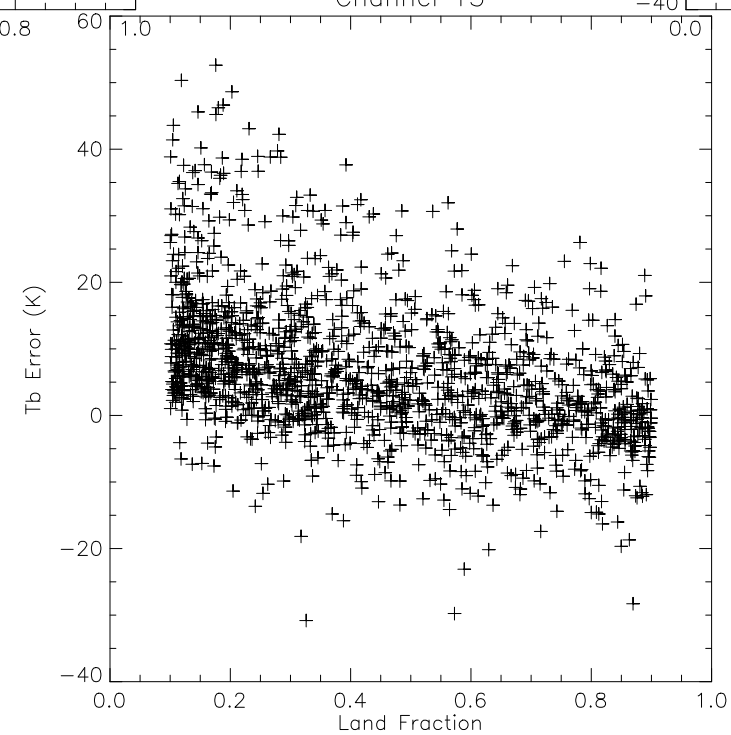
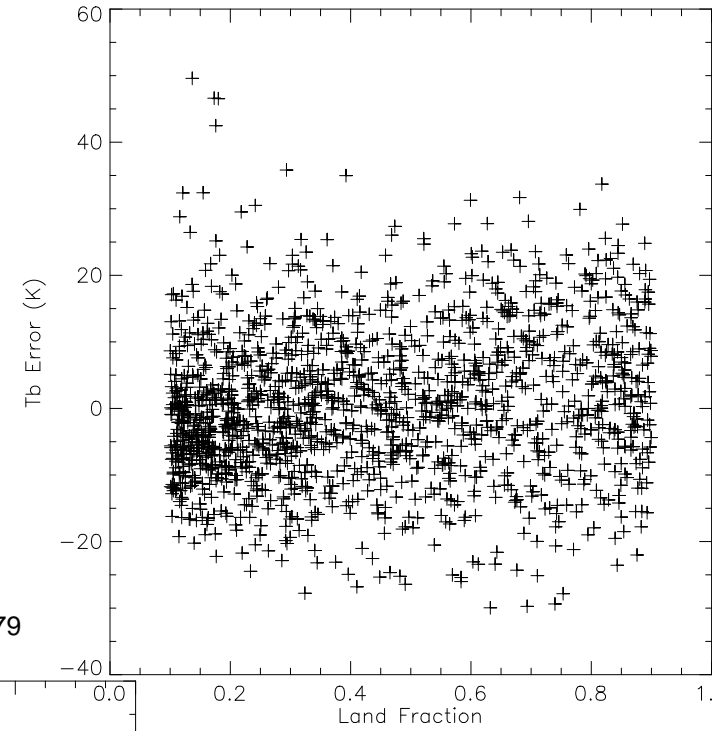
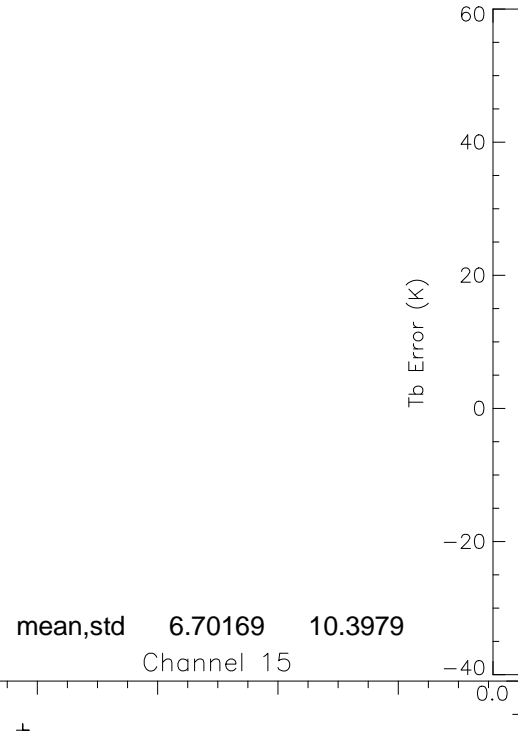
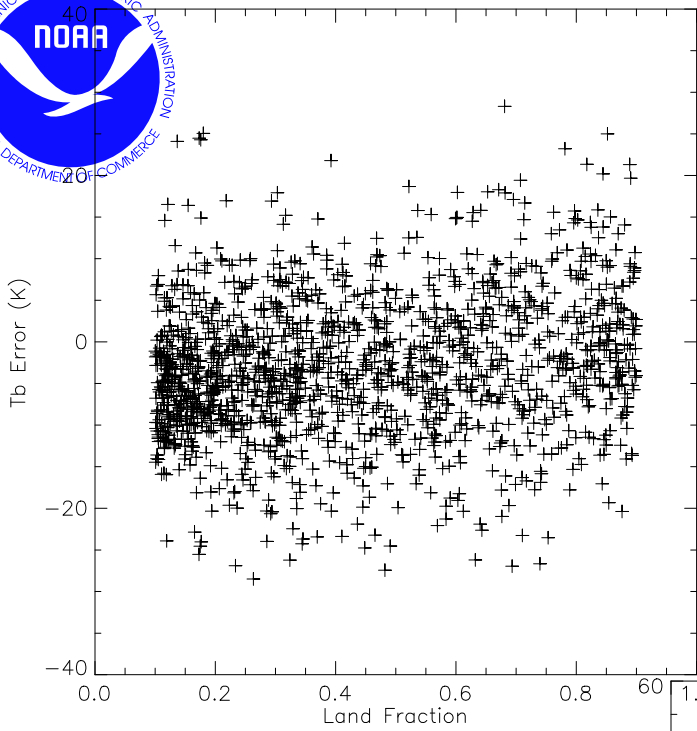
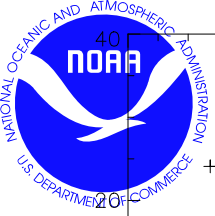
Channel 15

Land Mean -22.64 Stdev 15.65

Land Mean -28.41 Stdev 21.00



Tb Errors in coastlines
when assuming Ts is
land

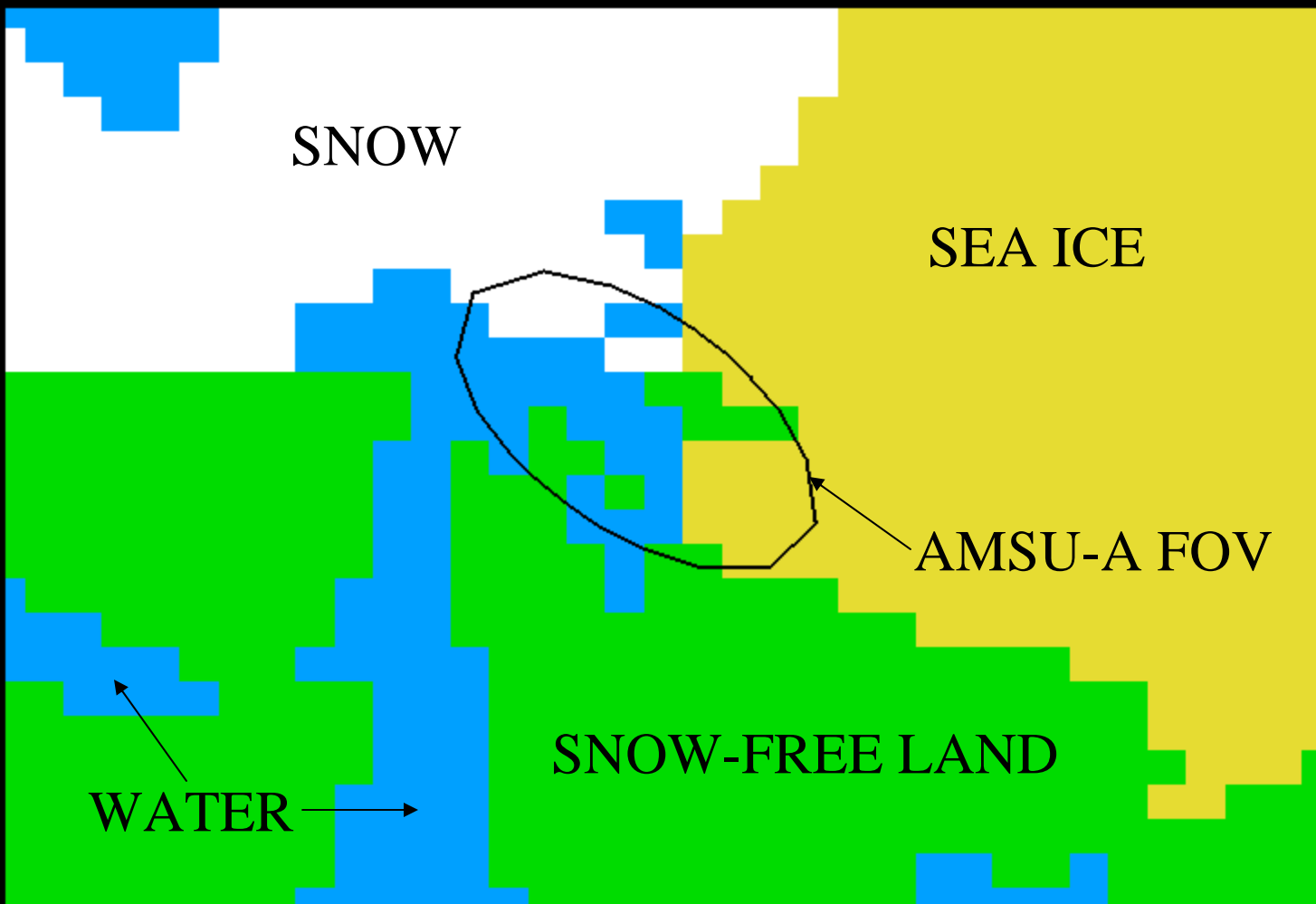


Tb Errors in coastlines
with mixed fov

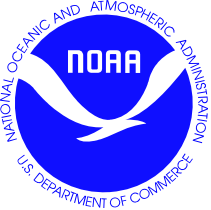


What does this look like just using GDAS within the fov?

- Use the above described methods to determine the various land/ water/ snow/ sea ice fractions and pass to CRTM
- Preliminary results in the following slides from George Gayno, NCEP/EMC/JCSDA/SAIC



MODEL MASK ~ 12KM

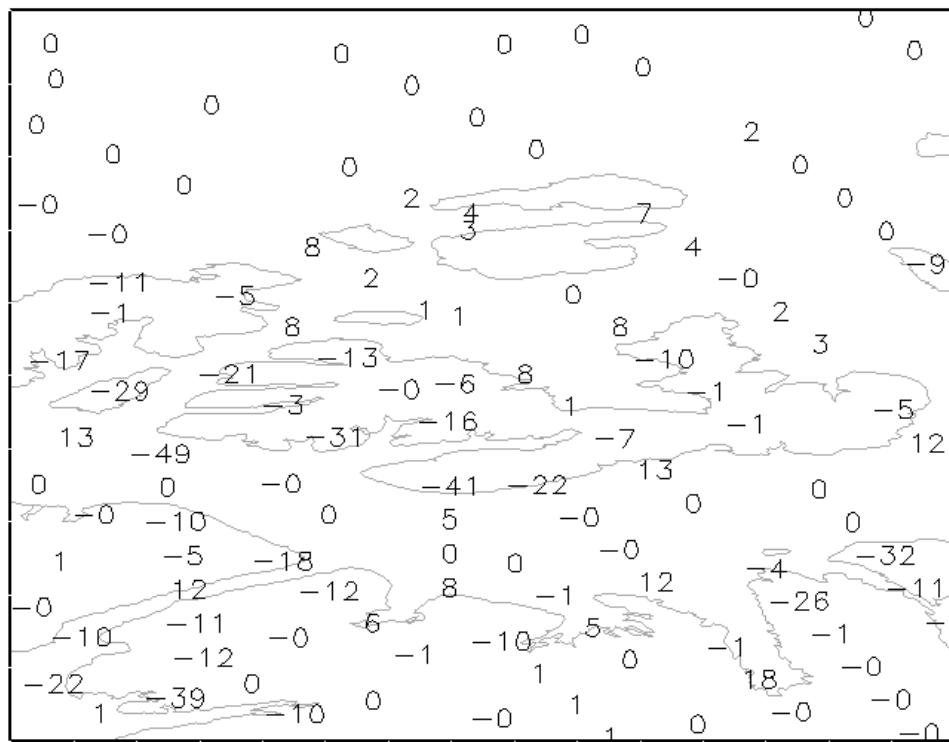
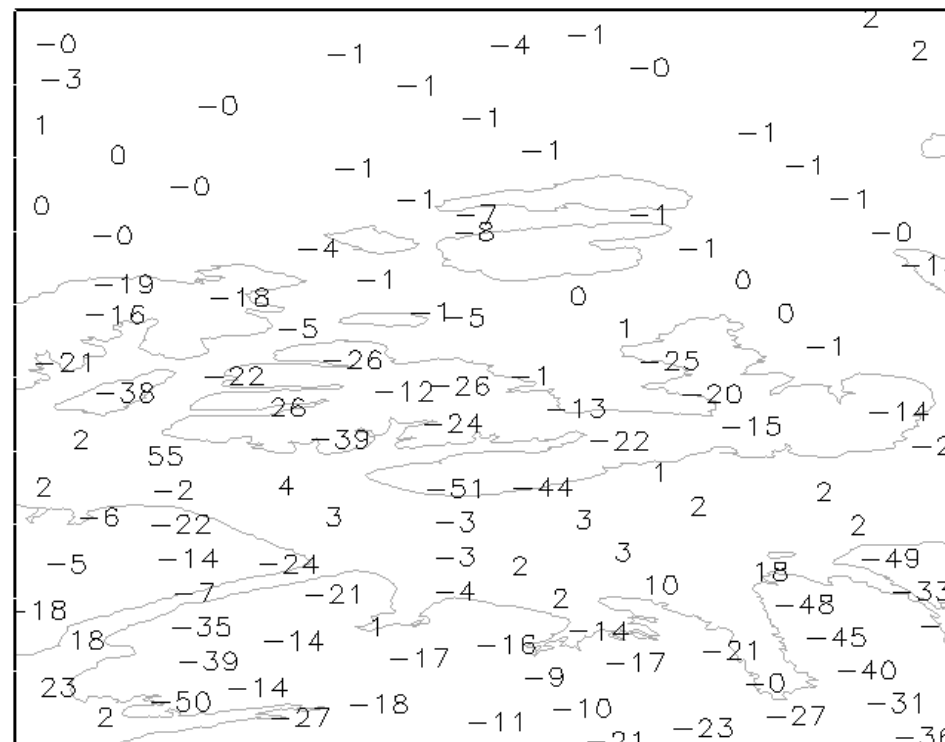


IMPACT: ACCOUNTING FOR FOV

EX: NOAA-15 AMSU-A, CHANNEL 2

CONTROL:
OBS. MINUS GUESS T_b

IMPACT: CHANGE IN
OBS. MINUS GUESS T_b



NORTHERN CANADA

NEGATIVE IS IMPROVEMENT



Potential Improvements

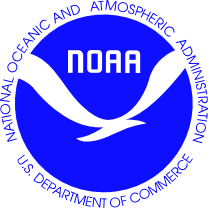
- Work shown here uses the nominal fov centroid zenith angle. It would be better to use the actual angles within the fov.
- Fit each channel independently
- Fit as a function of scan position
- ...

This is preliminary work

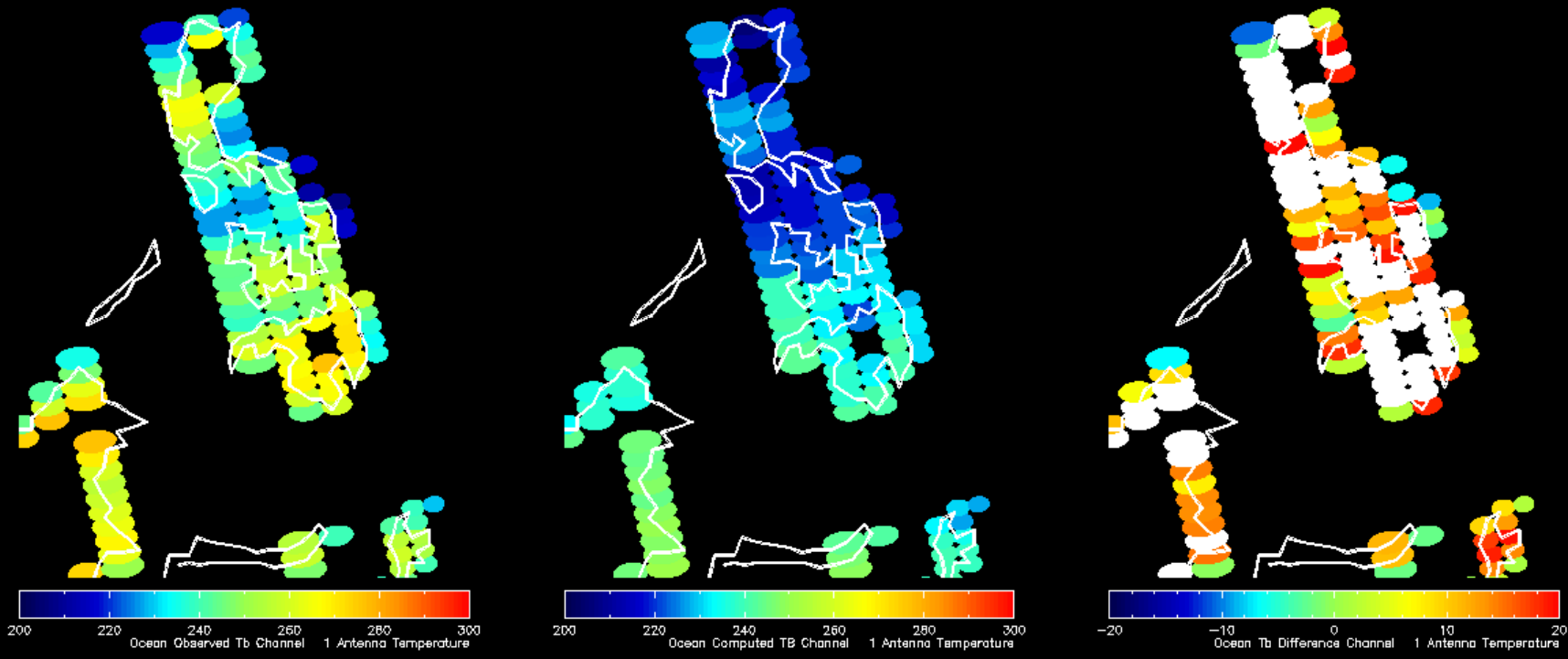


Summary and Discussion

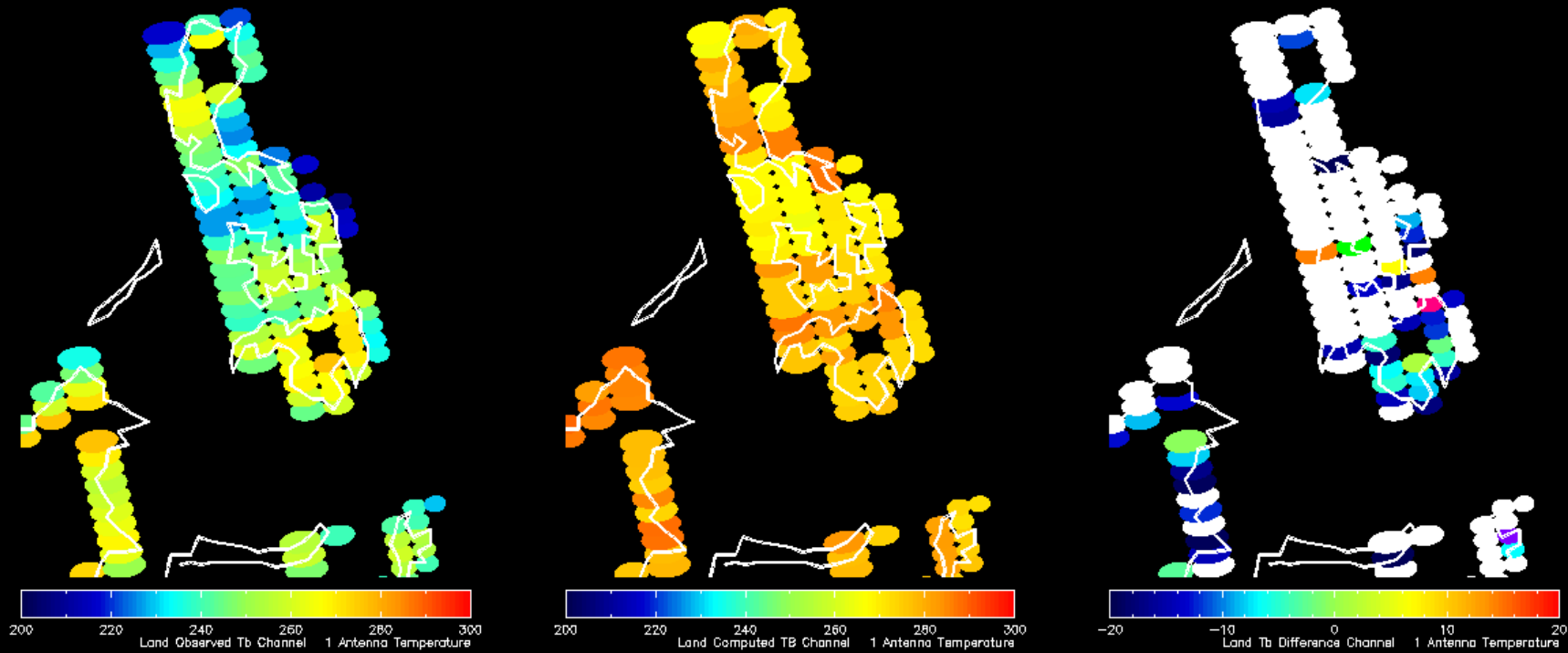
- A method has been presented to use sub-fov radiative transfer to improve radiances over inhomogeneous surfaces
- Usefulness of this technique is limited by the quality and resolution of available model state/ancillary databases
- Usefulness also limited by the expense of fov integration and multiple RT calculations
- Future application of Moore's law and other hardware development may ease these restrictions



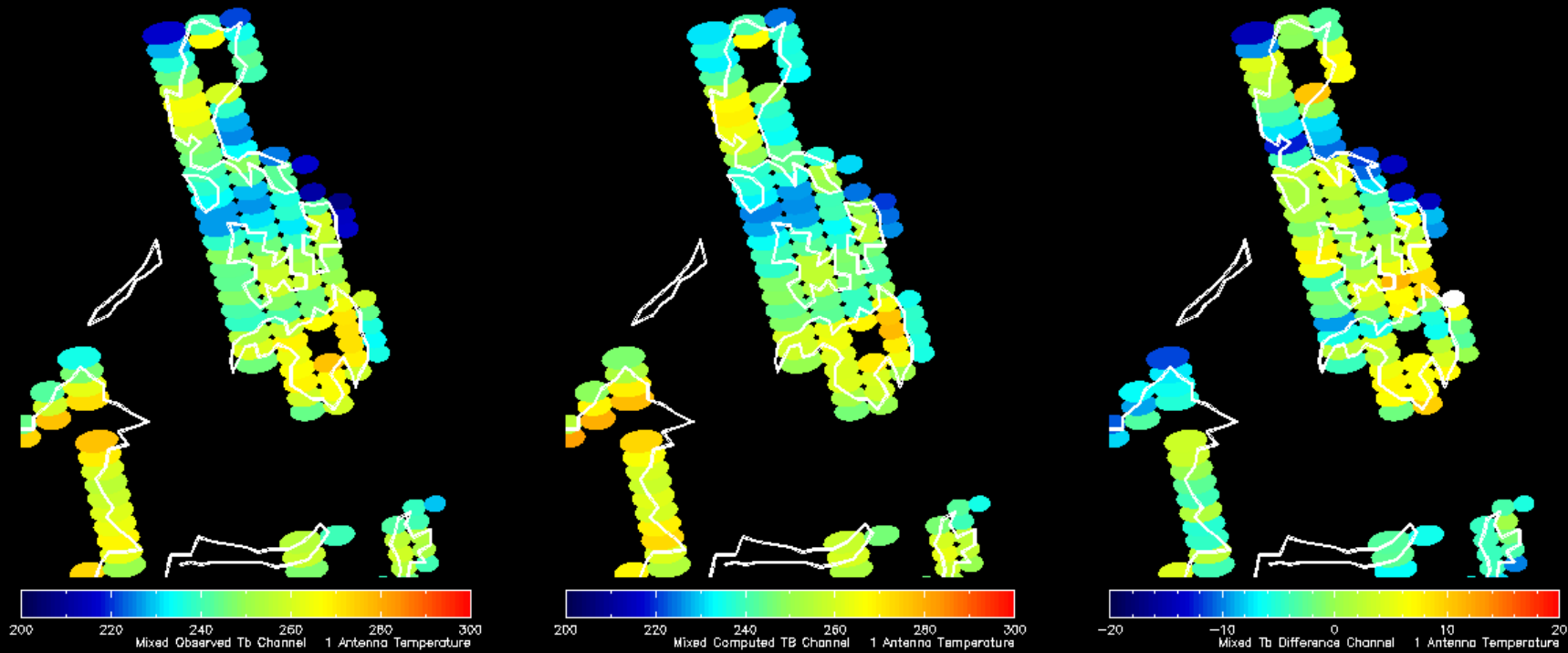
Back up slides



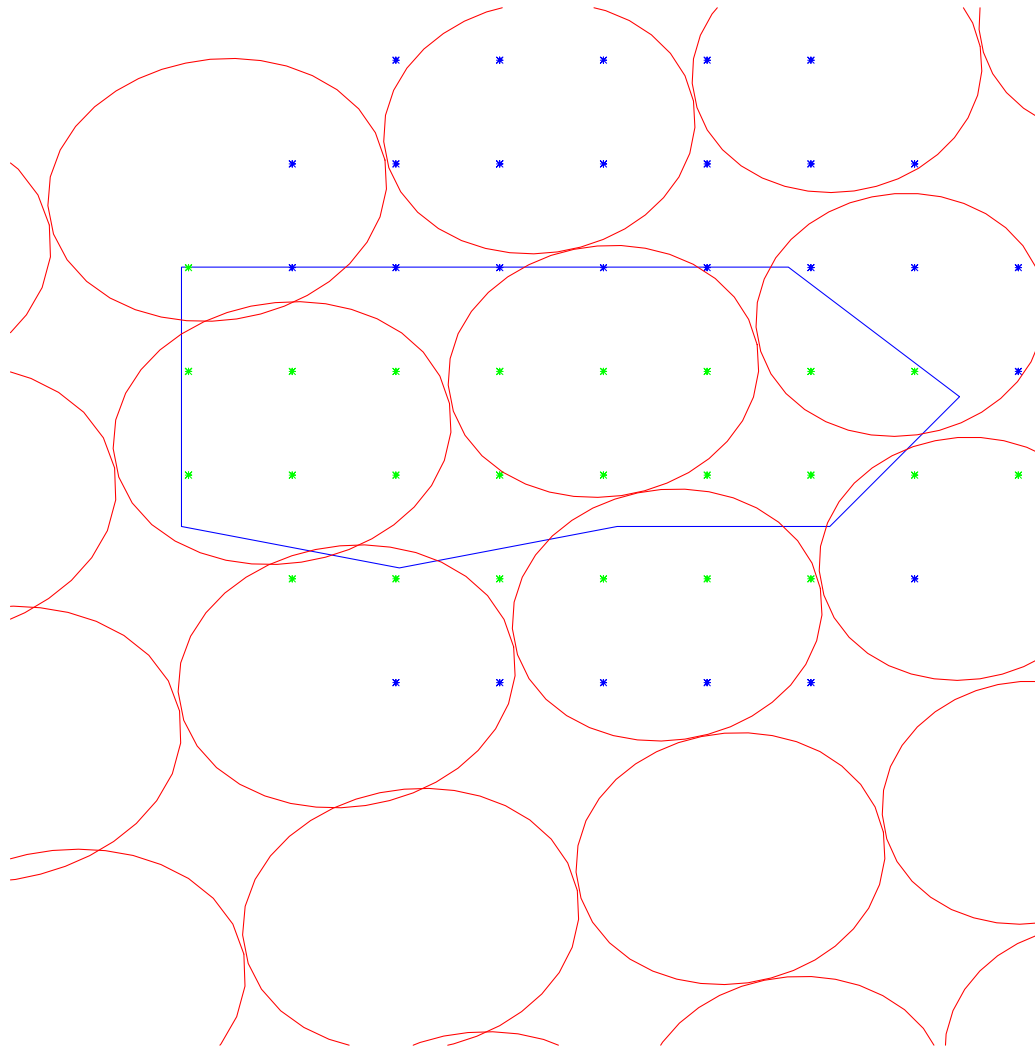
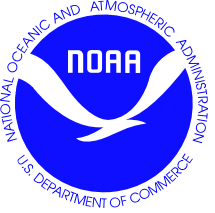
Ocean Temperature



Land temperature



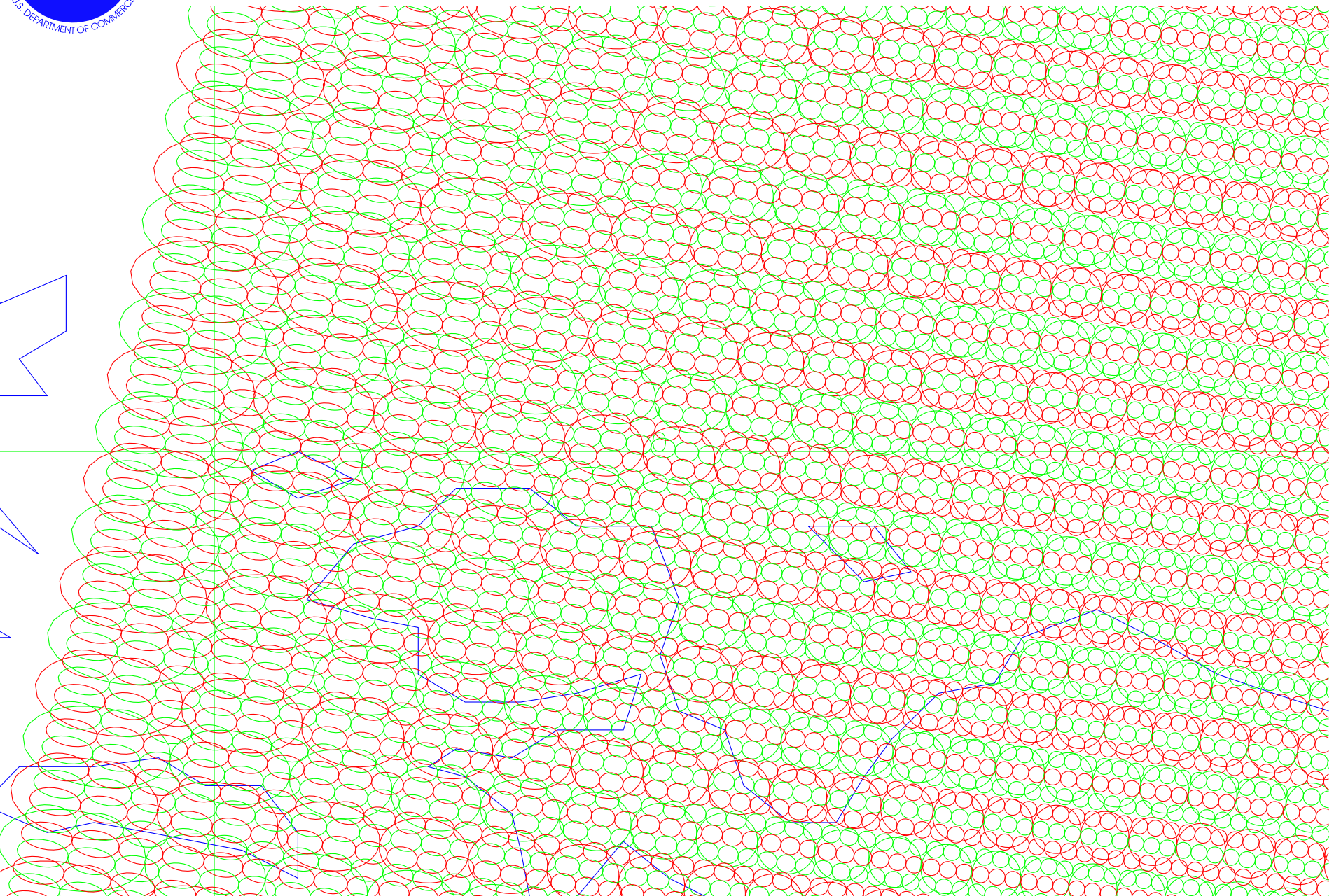
Mixed temperature

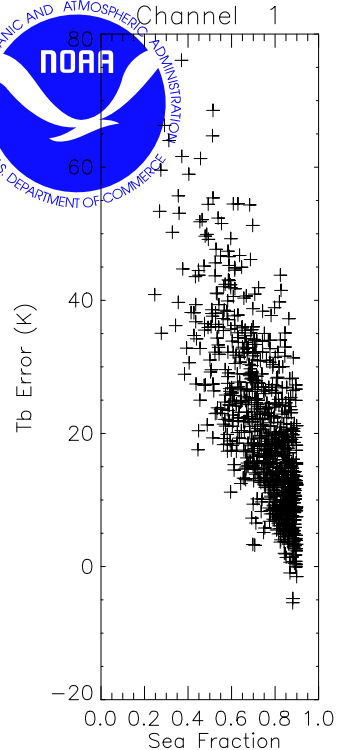
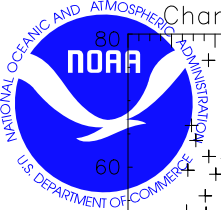


This is a first attempt with idl, using it's lores coastline (we don't have the CIA hires coastline, and using the F:\landsea\global.eighth, which is clearly not up to the task.

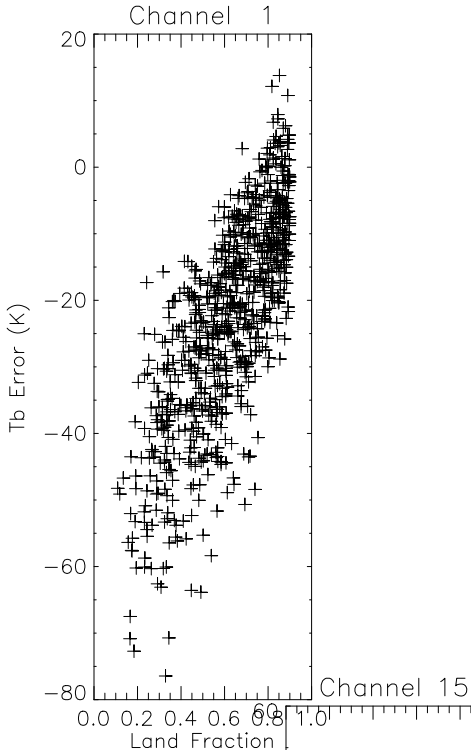


NOAA-17 AMSU-A and AMSU-B scan pattern in cylindrical coordinates. Coastline is North New Guinea.

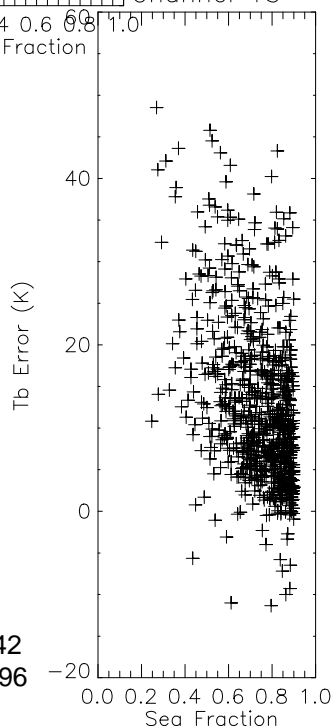




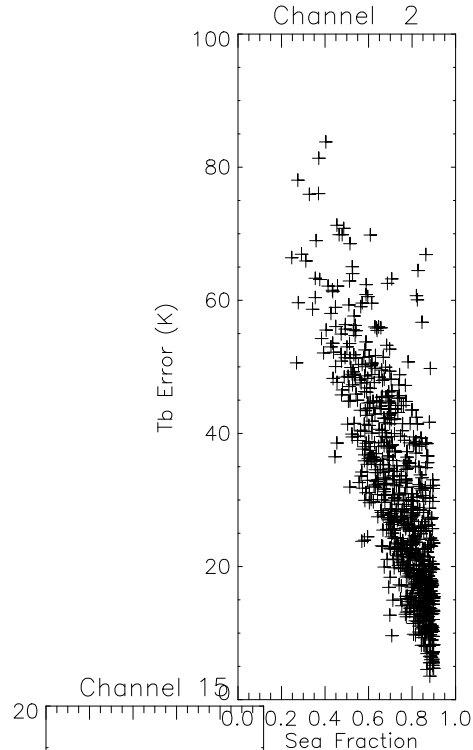
Sea Mean 20.5556 Stdev 12.5523
 Land Mean -22.6450 Stdev 15.6544



Channel 15



Sea Mean 12.3312 Stdev 9.39142
 Land Mean -11.5600 Stdev 8.81596



Sea Mean 29.4404 Stdev 15.1999
 Land Mean -28.4093 Stdev 20.9997

