

Tangent Linear and Adjoint Coding
Short Course
Day 2
Adjoint Coding

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Lessons Learned from Yesterday's TL

- **ALL input levels must be perturbed simultaneously in both TL and perturbed forward model**
- **The limit test is performed on output channel Tb_TL**
- **I suggest picking channels that reflect different physics:**
 - **1: a temperature sensitive channel, 2: a water vapor channel,**
 - **3: An ozone sensitive channel, 4: a window channel**
- **When in doubt, check all channels**

- **I had suggested passing forward variables through COMMON. Passing through calling parameters works just as well.**
- **Active variables for this problem are:**
 - **T, Tskin, tau, emiss**
 - **Make TL variables for all of these and differentiate.**
- **Who claims the the prize for first correct solution?**

Further Lessons Learned

Enter Class Comments here:

Review of Previous Day Problem Set

```
!Code excerpt from Compbright_Save_TL.f90
```

```
! named common saves intermediate forward model values for use in TL,AD,K codes
```

```
Real B(46,19),Bs(19),TotalRad(19)
```

```
Common /radiance/ B,Bs,TotalRad
```

```
Do ichan = 1 , M
```

```
! Initialize integrator
```

```
Sum_TL=0.
```

```
! Compute t1 radiance for first level
```

```
Call Planck_TL(Vnu(ichan),T(1),T_TL(1),B(1,Ichan),B_TL(1))
```

```
! Now compute radiances for the rest of the levels
```

```
Do level=2,N
```

```
Call Planck_TL(Vnu(ichan),T(level),T_TL(level),B(level,Ichan),B_TL(level))
```

```
! Sum=Sum+.5*(B1+B2)*(Tau1-Tau2) ! forward left commented in place
```

```
Sum_TL = Sum_TL +.5*(  
    (B_TL(level-1) +B_TL(level))*(Tau(level-1,ichan)-Tau(level,ichan)) &  
+ (B(level-1,ichan)+B(level,ichan))*(Tau_TL(level-1,ichan)-Tau_TL(level,ichan)) &  
    )
```

```
EndDo
```

```
! Surface term, ignoring downward reflected
```

```
Call Planck_TL(Vnu(ichan),Tskin,Tskin_TL,Bs(Ichan),Bs_TL)
```

```
!Sum=Sum+Bs*Tau(N,ichan)*Emiss(ichan) ! forward left commented in place
```

```
Sum_TL = Sum_TL + Bs_TL *Tau(N,ichan) *Emiss(ichan) &  
    + Bs(ichan) *Tau_TL(N,ichan)*Emiss(ichan) &  
    + Bs(ichan) *Tau(N,ichan) *Emiss_TL(ichan)
```

```
! Now brightness temperature
```

```
Tb_TL(ichan) = 0
```

```
If(TotalRad(Ichan).gt.0.) Then
```

```
Tb_TL(ichan) = Bright_TL(Vnu(ichan),TotalRad(Ichan),Sum_TL,BC1(ichan),BC2(ichan))
```

```
EndIf
```

```
EndDo ! ichan
```

```

! Code excerpt from Test_Compbright_Save_AD.f90
Do i = 1 , Niter ! outer loop emulates taking the limit
  Sign = -1.0
  Do isign = 1 , 2 ! inner loop delta x -> 0 +-

    Sign = -Sign

! compute perturbed basic state
    Call Compbright_Save(  Vnu,          &
                          T+Sign*T_TL,  &
                          Tau+Sign*Tau_TL, &
                          Tskin+Sign*Tskin_TL, &
                          Emiss+Sign*Emiss_TL, &
                          BC1,BC2,Nlevel,Nchan, &
                          TbP)

! compute forward model values and variables here for use with TL
    Call Compbright_Save(Vnu,T,Tau,Tskin,Emiss,BC1,BC2,Nlevel,Nchan,Tb)

    Call Compbright_Save_TL(Vnu,          &
                            T,Sign*T_TL, &
                            Tau,Sign*Tau_TL, &
                            Tskin,Sign*Tskin_TL, &
                            Emiss,Sign*Emiss_TL, &
                            BC1,BC2,Nlevel,Nchan, &
                            Tb,Tb_TL)

    Ratio(isign) = (TbP(Ichan) - Tb(Ichan) ) / Tb_TL(Ichan)          ! ratio

  EndDo ! sign

  Write(6,6120) i, Ratio(1),Ratio(2)

  TLIn =TLin*.5 ! halve perturbation

  EndDo ! iter
EndDo

```

Is this a bad result?

HIRS channel	5	Single precision
Iter	Pos ratio	Neg ratio
1	1.034600735	0.968000233
2	1.016974330	0.983676672
3	1.008406639	0.991757333
4	1.004179955	0.995861471
5	1.002081037	0.997931898
6	1.001035571	0.998961031
7	1.000512838	0.999500036
8	1.000218749	0.999761403
9	1.000088096	0.999826789
10	0.999957442	1.000218749
11	0.999957442	0.999957442
12	0.999434710	1.000480175
13	0.999434710	1.001525640
14	0.995252967	1.003616452
15	0.995252967	1.003616452

Ratio starts to wander at iteration 10

HIRS channel	5	Double Precision
Iter	Pos ratio	Neg ratio
1	1.034600773	0.968000178
2	1.016974788	0.983675551
3	1.008406038	0.991756553
4	1.004182687	0.995857961
5	1.002086261	0.997923901
6	1.001041860	0.998960680
7	1.000520613	0.999480023
8	1.000260227	0.999739932
9	1.000130094	0.999869946
10	1.000065042	0.999934968
11	1.000032520	0.999967483
12	1.000016260	0.999983741
13	1.000008130	0.999991870
14	1.000004065	0.999995935
15	1.000002032	0.999997968

Double precision reveals that wandering is a precision issue.

This passes the limit test.

Remember: direction of approach for pos and neg ratio may vary from variable to variable.

Check each variable class.

What good are adjoints?

If your pickup is broken, your girl has left you, and your dog has died:

Using adjoint techniques, you can :

- **fix your pickup,**
- **get your girl back,**
- **and bring your dog back to life, as long as they have been properly linearized. (at least in theory)**

Adjoint coding objective

- **To make the linearized code run backwards.**
- **E.g.: TL code inputs linearized temperature profile and outputs linearized brightness temperature**
- **Adjoint code inputs linearized brightness temperatures and outputs linearized temperature profile**
- **Note that I often interchange ‘linearized’ and ‘derivative’**

Our objective is the Jacobian

$$\mathbf{K}(\mathbf{x})^T = \begin{bmatrix} \frac{\partial \mathbf{R}_1}{\partial \mathbf{T}_1} & \frac{\partial \mathbf{R}_2}{\partial \mathbf{T}_1} & \frac{\partial \mathbf{R}_3}{\partial \mathbf{T}_1} & \dots & \frac{\partial \mathbf{R}_m}{\partial \mathbf{T}_1} \\ \frac{\partial \mathbf{R}_1}{\partial \mathbf{R}_1} & \frac{\partial \mathbf{R}_2}{\partial \mathbf{R}_2} & \frac{\partial \mathbf{R}_3}{\partial \mathbf{R}_3} & \dots & \frac{\partial \mathbf{R}_m}{\partial \mathbf{R}_m} \\ \frac{\partial \mathbf{T}_2}{\partial \mathbf{T}_2} & \frac{\partial \mathbf{T}_2}{\partial \mathbf{T}_2} & \frac{\partial \mathbf{T}_2}{\partial \mathbf{T}_2} & \dots & \frac{\partial \mathbf{T}_2}{\partial \mathbf{T}_2} \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ \frac{\partial \mathbf{R}_1}{\partial \mathbf{R}_1} & \frac{\partial \mathbf{R}_2}{\partial \mathbf{R}_2} & \frac{\partial \mathbf{R}_3}{\partial \mathbf{R}_3} & \dots & \frac{\partial \mathbf{R}_m}{\partial \mathbf{R}_m} \\ \frac{\partial \mathbf{T}_n}{\partial \mathbf{R}_1} & \frac{\partial \mathbf{T}_n}{\partial \mathbf{R}_2} & \frac{\partial \mathbf{T}_n}{\partial \mathbf{R}_3} & \dots & \frac{\partial \mathbf{T}_n}{\partial \mathbf{R}_m} \\ \frac{\partial \mathbf{q}_1}{\partial \mathbf{R}_1} & \frac{\partial \mathbf{q}_1}{\partial \mathbf{R}_2} & \frac{\partial \mathbf{q}_1}{\partial \mathbf{R}_3} & \dots & \frac{\partial \mathbf{q}_1}{\partial \mathbf{R}_m} \\ \frac{\partial \mathbf{q}_2}{\partial \mathbf{R}_1} & \frac{\partial \mathbf{q}_2}{\partial \mathbf{R}_2} & \frac{\partial \mathbf{q}_2}{\partial \mathbf{R}_3} & \dots & \frac{\partial \mathbf{q}_2}{\partial \mathbf{R}_m} \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ \frac{\partial \mathbf{R}_1}{\partial \mathbf{R}_1} & \frac{\partial \mathbf{R}_2}{\partial \mathbf{R}_2} & \frac{\partial \mathbf{R}_3}{\partial \mathbf{R}_3} & \dots & \frac{\partial \mathbf{R}_m}{\partial \mathbf{R}_m} \\ \frac{\partial \mathbf{q}_n}{\partial \mathbf{R}_1} & \frac{\partial \mathbf{q}_n}{\partial \mathbf{R}_2} & \frac{\partial \mathbf{q}_n}{\partial \mathbf{R}_3} & \dots & \frac{\partial \mathbf{q}_n}{\partial \mathbf{R}_m} \end{bmatrix}$$

Recommended AD Naming Conventions

There is no ‘standard’ naming convention. Here is what I recommend:

- **Keep forward model variable names the same**
- **Append “_AD” to forward model variable and routine names to describe adjoint variables and routines**

How do we derive the Adjoint Code

- **By taking the transpose of the Tangent Linear Code**
- **It's that simple.**

Huh?

Well, maybe it's not quite that simple.

Adjoint Coding Rules

- **Call forward model first to initialize forward variables**
- **Reverse the order of TL routine calls**
- **Convert Functions to Subroutines**
- **Reverse the order of active loop indices**
- **Reverse the order of code within loops and routines**
- **Reverse the inputs and outputs of assignment statements**
- **Accumulate the outputs of the assignment statements**
- **Rename TL variables and routines to AD**

- **Initializing output accumulators is VERY important**

Example 1: reverse order of routines

TL

Program Main_TL

Call Sub1

Call Sub2

Call Sub3

Call Sub1_TL

Call Sub2_TL

Call Sub3_TL

End Program Main_TL

Adjoint

Program Main_AD

Call Sub1

Call Sub2

Call Sub3

Call Sub3_AD

Call Sub2_AD

Call Sub1_AD

End Program Main_AD

Example 2: Functions to Subroutines

Reverse code order, reverse assignment I/O&accumulate

TL

Real Function Bright_TL

(V,Radiance,Radiance_TL,BC1,BC2)

$K2 = C2 * V$

$K1 = C1 * V * V * V$

TempTb_TL =

$K2 * Alog(K1/Radiance + 1.) ** (-2.)$
 $* Radiance_TL / (K1 + Radiance) *$
 $K1 / Radiance$ (1)

Bright_TL = BC2 * TempTb_TL (2)

Return

End Function Bright_TL

Adjoint

Subroutine Bright_AD

(V,Radiance,Radiance_AD,BC1,
BC2,**Tb_AD**)

$K2 = C2 * V$

$K1 = C1 * V * V * V$ **!inactive constants**

TempTb_AD = 0 ! initialize for each invocation

TempTb_AD = TempTb_AD +
BC2 * **Tb_AD** (2)

Radiance_AD = Radiance_AD +

$K2 * Alog(K1/Radiance + 1.) ** (-2.)$
 $* TempTb_AD / (K1 + Radiance) *$
 $K1 / Radiance$ (1)

Return

End Subroutine Bright_AD

Example 3 – from Compbright_AD: Reverse inputs and outputs of assignments

1

2

```
Sum_TL = Sum_TL + Bs_TL *Tau(N,ichan) *Emiss(ichan) &
          + Bs(ichan) *Tau3_TL(N,ichan) *Emiss(ichan) &
          + Bs(ichan) *Tau(N,ichan) *Emiss_TL(ichan)
4
```

Sum_AD = Sum_AD ! Doesn't do anything, we can toss this statement

```
Bs_AD = Bs_AD + Sum_AD *Tau(N,ichan)*Emiss(ichan)
Tau_AD(N,ichan)= Tau_AD(N,ichan) + Bs(ichan) *Sum_AD *Emiss(ichan)
Emiss_AD(ichan)= Emiss_AD(ichan) + Bs(ichan) *Tau(N,ichan)*Sum_AD
```

Accumulate

Reverse inputs and outputs

Example 3 revisited ala G&K pg 12

m is the current realization of the values

$$\mathbf{TL} \quad \begin{bmatrix} \text{sum}' \\ \mathbf{B}_s' \\ \tau' \\ \varepsilon' \end{bmatrix}^m = \begin{bmatrix} 1 & \tau'\varepsilon' & \mathbf{B}_s'\varepsilon' & \mathbf{B}_s'\tau' \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \text{sum}' \\ \mathbf{B}_s' \\ \tau' \\ \varepsilon' \end{bmatrix}^{m-1}$$

Taking the transpose

$$\mathbf{AD} \quad \begin{bmatrix} \text{sum}' \\ \mathbf{B}_s' \\ \tau' \\ \varepsilon' \end{bmatrix}^{m-1*} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ \tau'\varepsilon' & 1 & 0 & 0 \\ \mathbf{B}_s'\varepsilon' & 0 & 1 & 0 \\ \mathbf{B}_s'\tau' & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \text{sum}' \\ \mathbf{B}_s' \\ \tau' \\ \varepsilon' \end{bmatrix}^{m*}$$

Example 4: Reverse indexing of loops

```
TL      Do I = 1 , Nlevel
          B_Tl(I) = T_TL(I)*Tau(I) + T(I)*Tau_TL(I)
        EndDo
```

```
AD      Do I = Nlevel, 1 , -1
          T_AD(I) = T_AD(I) + B_AD(I)*Tau(I)
          Tau_AD(I) = Tau_AD(I) + T(I)*B_AD(I)
        EndDo
```

This illustrates reversing loop flow. Doesn't make any difference for this particular code fragment, but in general it does.

Initializing Accumulators

G&K say zero accumulators after done using them.

However, you have to zero them before you use them the first time, so just zero them before you start.

AD variables local to a routine should be zeroed there.

Adjoint testing

- **Objective:** Assure that the adjoint is the transpose of the tangent linear
- **Method:** Construct Jacobians from TL and AD and compare

N inputs -> TL -> M outputs

M inputs -> AD -> N outputs

Call TL N times with the i th element=1, all other elements =0

Put output into i th row of an $N \times M$ array

Call AD M times with the j th element=1, all other elements=0

Put output into a j th row of an $M \times N$ array

Verify that $AD = TL^T$ to within machine precision

Tangent-Linear Output

$$\mathbf{K}(\mathbf{X}) = \left[\begin{array}{cccc} \frac{\partial \mathbf{R}_1}{\partial \mathbf{X}} & \frac{\partial \mathbf{R}_2}{\partial \mathbf{X}} & \frac{\partial \mathbf{R}_3}{\partial \mathbf{X}} & \dots \frac{\partial \mathbf{R}_m}{\partial \mathbf{X}} \end{array} \right]$$

For a single call to TL, output is derivative of each channel radiance with respect to whole input state vector.

Adjoint Output

$$\mathbf{K}(\mathbf{x})^T = \begin{bmatrix} \frac{\partial \mathcal{R}}{\partial T_1} \\ \frac{\partial \mathcal{R}}{\partial T_2} \\ \vdots \\ \frac{\partial \mathcal{R}}{\partial T_n} \\ \frac{\partial \mathcal{R}}{\partial q_1} \\ \frac{\partial \mathcal{R}}{\partial q_2} \\ \vdots \\ \frac{\partial \mathcal{R}}{\partial q_n} \end{bmatrix}$$

For a single call to AD, output is derivative of all channel radiances with respect to each element of the input state vector.

Filling the Jacobian

We call the TL and AD with all input elements set to zero except one so as to isolate the derivative to a specific element of the Jacobian. This gives the derivative

$$\frac{\partial R_j}{\partial x_i}$$

TL Jacobian Construction

$$\mathbf{K}(\mathbf{x}_1) = \begin{bmatrix} \frac{\partial \mathbf{R}_1}{\partial \mathbf{x}_1} & \frac{\partial \mathbf{R}_2}{\partial \mathbf{x}_1} & \frac{\partial \mathbf{R}_3}{\partial \mathbf{x}_1} & \dots & \frac{\partial \mathbf{R}_m}{\partial \mathbf{x}_1} \end{bmatrix}$$

$$\mathbf{K}(\mathbf{x}_2) = \begin{bmatrix} \frac{\partial \mathbf{R}_1}{\partial \mathbf{x}_2} & \frac{\partial \mathbf{R}_2}{\partial \mathbf{x}_2} & \frac{\partial \mathbf{R}_3}{\partial \mathbf{x}_2} & \dots & \frac{\partial \mathbf{R}_m}{\partial \mathbf{x}_2} \end{bmatrix}$$

⋮

$$\mathbf{K}(\mathbf{x}_n) = \begin{bmatrix} \frac{\partial \mathbf{R}_1}{\partial \mathbf{x}_n} & \frac{\partial \mathbf{R}_2}{\partial \mathbf{x}_n} & \frac{\partial \mathbf{R}_3}{\partial \mathbf{x}_n} & \dots & \frac{\partial \mathbf{R}_m}{\partial \mathbf{x}_n} \end{bmatrix}$$

AD Jacobian Construction

$$\mathbf{K}_1(\mathbf{x})^T = \begin{bmatrix} \frac{\partial R_1}{\partial T_1} \\ \frac{\partial R_1}{\partial R_1} \\ \frac{\partial T_2}{\partial R_1} \\ \vdots \\ \frac{\partial T_n}{\partial R_1} \\ \frac{\partial R_1}{\partial q_1} \\ \frac{\partial R_1}{\partial q_2} \\ \vdots \\ \frac{\partial R_1}{\partial q_n} \end{bmatrix}, \mathbf{K}_2(\mathbf{x})^T = \begin{bmatrix} \frac{\partial R_2}{\partial T_1} \\ \frac{\partial R_2}{\partial R_2} \\ \frac{\partial T_2}{\partial R_2} \\ \vdots \\ \frac{\partial T_n}{\partial R_2} \\ \frac{\partial R_2}{\partial q_1} \\ \frac{\partial R_2}{\partial q_2} \\ \vdots \\ \frac{\partial R_2}{\partial q_n} \end{bmatrix}, \dots, \mathbf{K}_m(\mathbf{x})^T = \begin{bmatrix} \frac{\partial R_m}{\partial T_1} \\ \frac{\partial R_m}{\partial R_m} \\ \frac{\partial T_2}{\partial R_m} \\ \vdots \\ \frac{\partial T_n}{\partial R_m} \\ \frac{\partial R_m}{\partial q_1} \\ \frac{\partial R_m}{\partial q_2} \\ \vdots \\ \frac{\partial R_m}{\partial q_n} \end{bmatrix}$$

Machine Precision Considerations

Test that

$$\text{Abs}(TL-AD)/TL < MP$$

Rule of thumb:

MP = 1.e-7 for Single precision

MP = 1.e-12 for Double precision

Use errors intelligently

- **If the $AD \neq TL^T$, use the location in the matrix to find the error in the code.**
- **E.G. if $Tsfc_AD \neq Tsfc_T^T$, look where $Tsfc_AD$ is computed for the error.**
- **Make sure AD variables are initialized to zero.**

Adjoint Testing Example

```
! Compute forward model radiance

Call Planck(Vnu(Ichan),Temp,B)

! Compute TL values
Temp_TL = 1.0    ! Initialize input
B_TL = 0.0       ! Initialize output

Call Planck_TL(Vnu(Ichan),Temp,Temp_TL,B,B_TL) ! tangent linear model

! Compute AD values
B_AD = 1.0       ! Initialize input
Temp_AD = 0.0    ! Initialize output (accumulator)
Call Planck_AD(Vnu(Ichan),Temp,Temp_AD,B,B_AD) ! Adjoint model

! Here the output of the TL is 1x1 and the output of the AD is 1x1,
! so Transpose(TL) = AD ==> B_TL = Temp_AD

Write(6,*) B_TL, Temp_AD, B_TL-Temp_AD
```

Problem Set for Tomorrow:

Construct routine `COMPBRIGHT_SAVE_AD.F90` from TL code `COMPBRIGHT_TL_SAVE.F90` and test using techniques learned today.

Low level routines `PLANCK.F90`, `BRIGHT.F90`, `PLANCK_TL.F90`, `Bright_AD.F90`, `Planck_AD.F90`, `Bright_AD.F90`, `COMPBRIGHT_SAVE.F90` and `COMPBRIGHT_SAVE_TL.FOR`

and their testing routines are provided.

Hint: use of EQUIVALENCE greatly eases the testing.

```
! TL input vector
Equivalence (TLin(1  ), T_TL      )
Equivalence (TLin(47 ), Tau_TL    )
Equivalence (TLin(921), Emiss_TL  )
Equivalence (TLin(940), Tskin_TL  )

! AD output vector
Equivalence (ADout(1  ), T_AD      )
Equivalence (ADout(47 ), Tau_AD    )
Equivalence (ADout(921), Emiss_AD  )
Equivalence (ADout(940), Tskin_AD  )

Real Tb      (Nchan)    ! brightness temperature
Real Tb_TL(nTLout)    ! brightness temperature TL
Real Tb_AD(nADin)     ! brightness temperature AD

Real TLout(nTLout)
Real ADin (nADin)

Equivalence(TLout, Tb_TL)
Equivalence(ADin, Tb_AD)

Real TL(nTLin, nTLout)
Real AD(nADin, nADout)
```


Problem Set for Tomorrow cont:

Things to watch out for:

If test fails, don't assume that it is in the AD code... it could be in the testing logic.

Remember to zero outputs (accumulators).

Only set one input element to unity at a time. Rest are set to zero.

I find that maybe half of the errors that I chase down are in the testing logic.

Don't wait to do this assignment.
It is difficult.

Good fun and have luck.